
Influence of PWM Inverters on Bearing Currents

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Scope

- Introduction
 - PWM Inverter Topology
 - Common Mode Voltage and Shaft Voltage
- Factors Affecting Shaft Voltage and Bearing Current
- Study of Bearing Insulation Characteristics
When Subjected to Externally Injected Signal
- Techniques to Reduce Bearing Current Issues Caused by
PWM Inverters

1. 2-Level PWM Inverter Topology

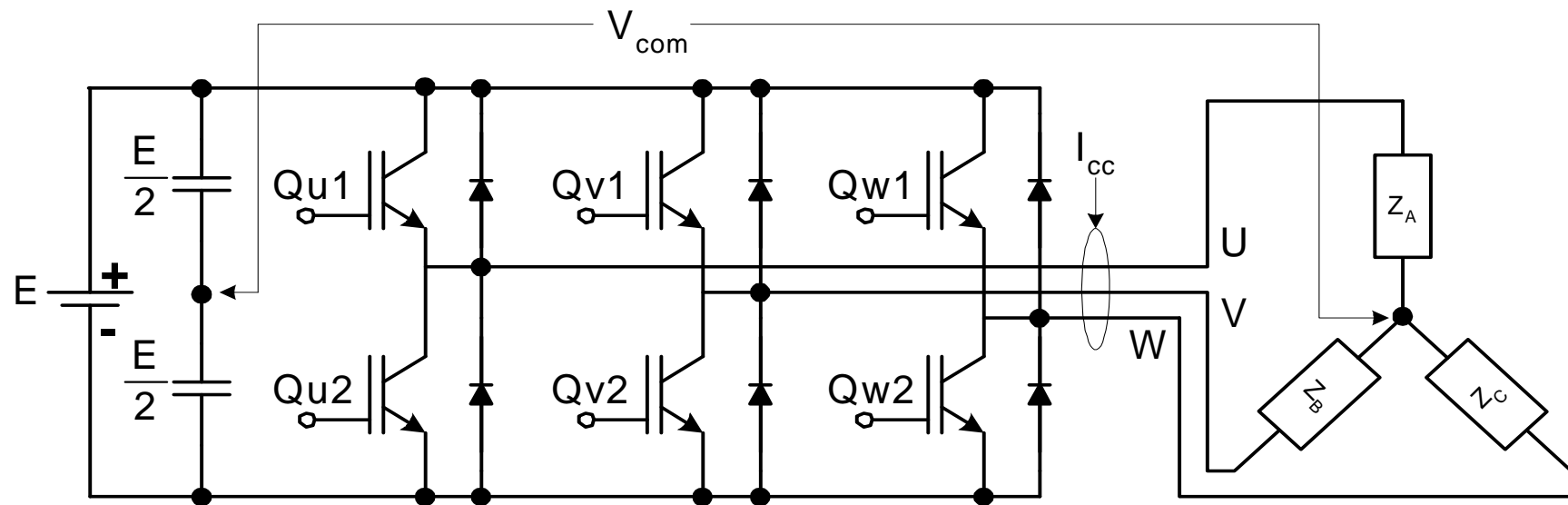


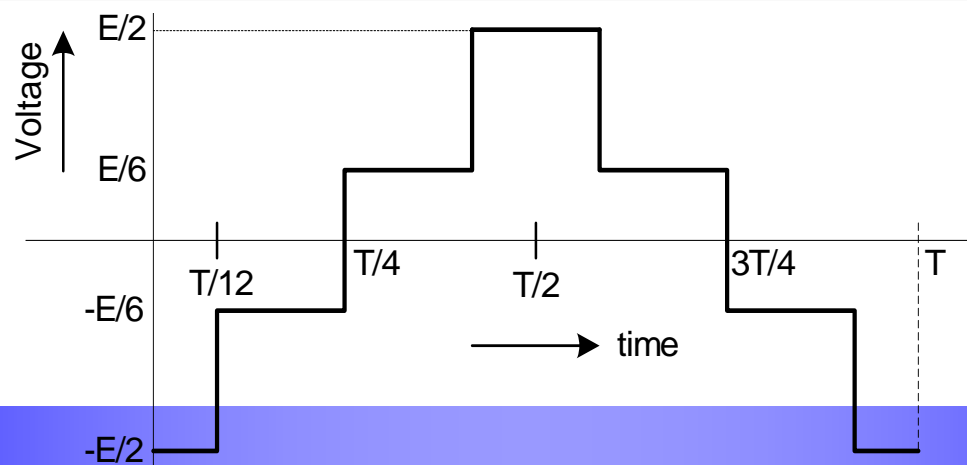
Table 1. Relation between switching states and output voltage

	Q_{u1}	Q_{u2}	V_u
Switching State	ON	OFF	$+E/2$
	OFF	ON	$-E/2$

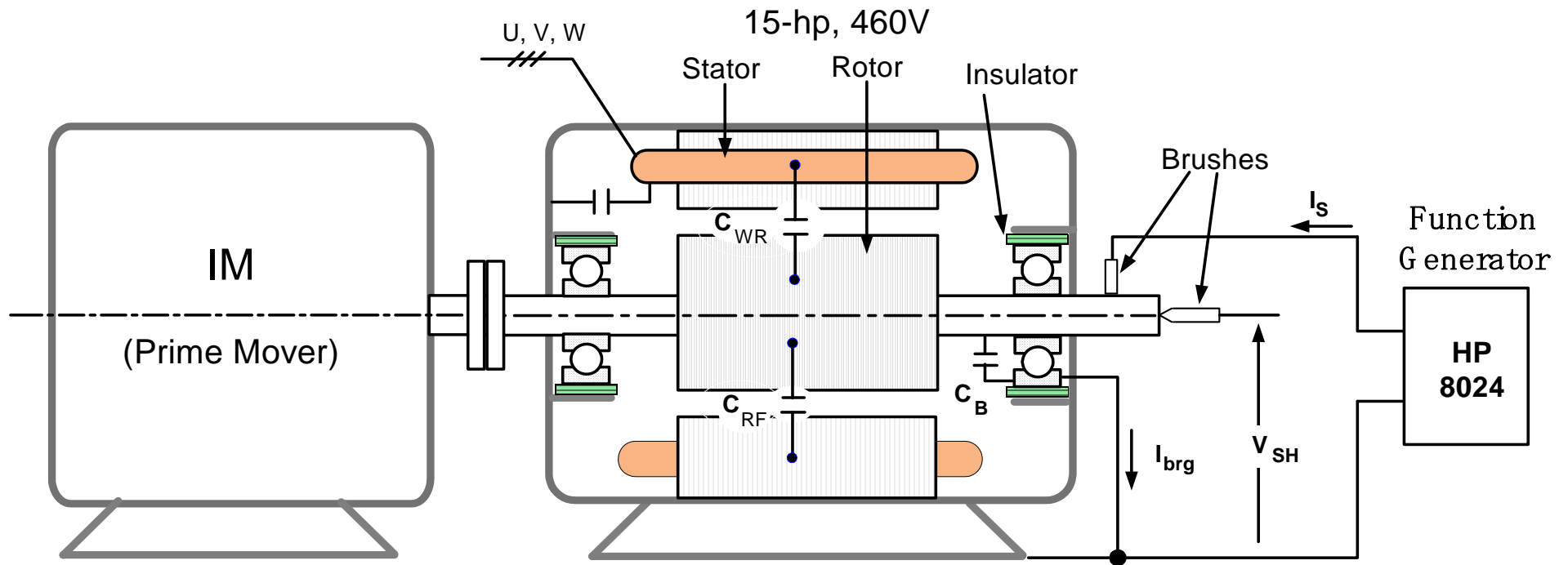
1. Common Mode Voltage in 2-Level Inverters

Table 1. Relation between switching states and output voltage

	Q_{u1}	Q_{u2}	Q_{v1}	Q_{v2}	Q_{w1}	Q_{w2}	V_{com}
Switching State	OFF	ON	OFF	ON	OFF	ON	$-E/2$
	ON	OFF	OFF	ON	OFF	ON	$-E/6$
	ON	OFF	ON	OFF	OFF	ON	$+E/6$
	ON	OFF	ON	OFF	ON	OFF	$+E/2$
	OFF	ON	ON	OFF	ON	OFF	$+E/6$
	OFF	ON	OFF	ON	ON	OFF	$-E/6$
	OFF	ON	OFF	ON	OFF	ON	$-E/2$

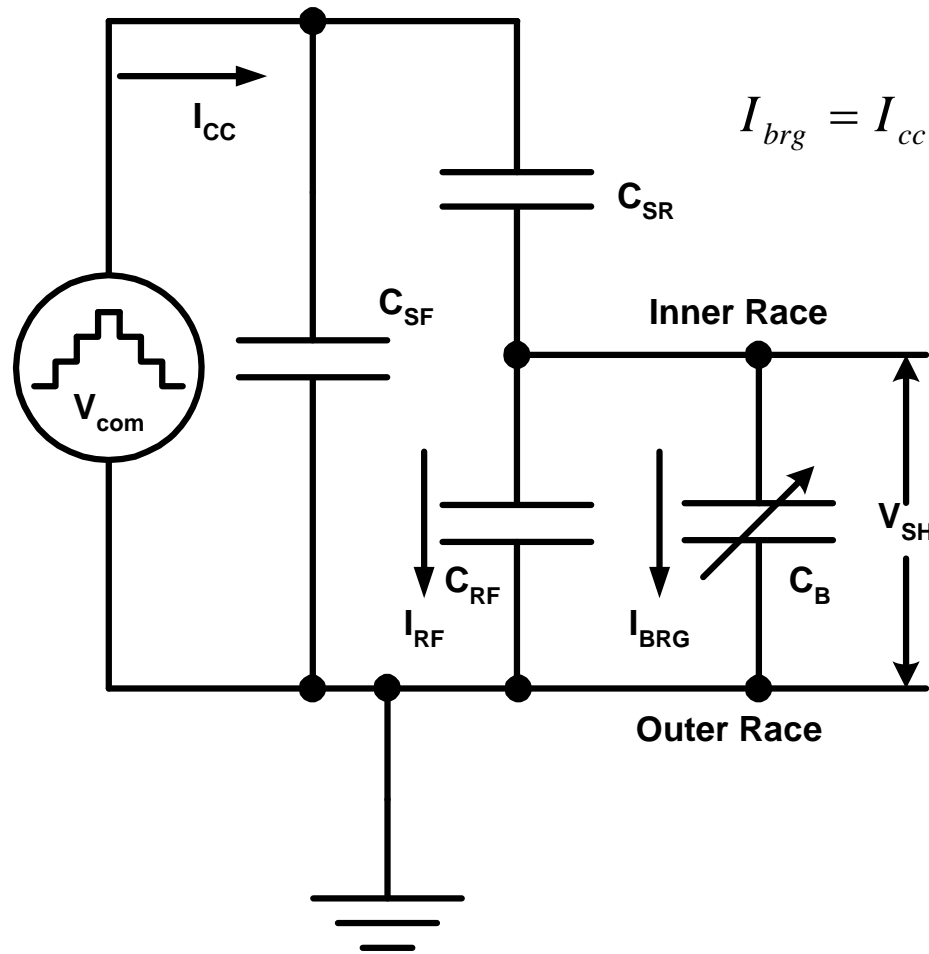


2. Test Setup



- Test motor – driven by another motor
- Waveforms applied from Function Generator to study bearing breakdown phenomenon

3. Parasitic Model for Bearing Test

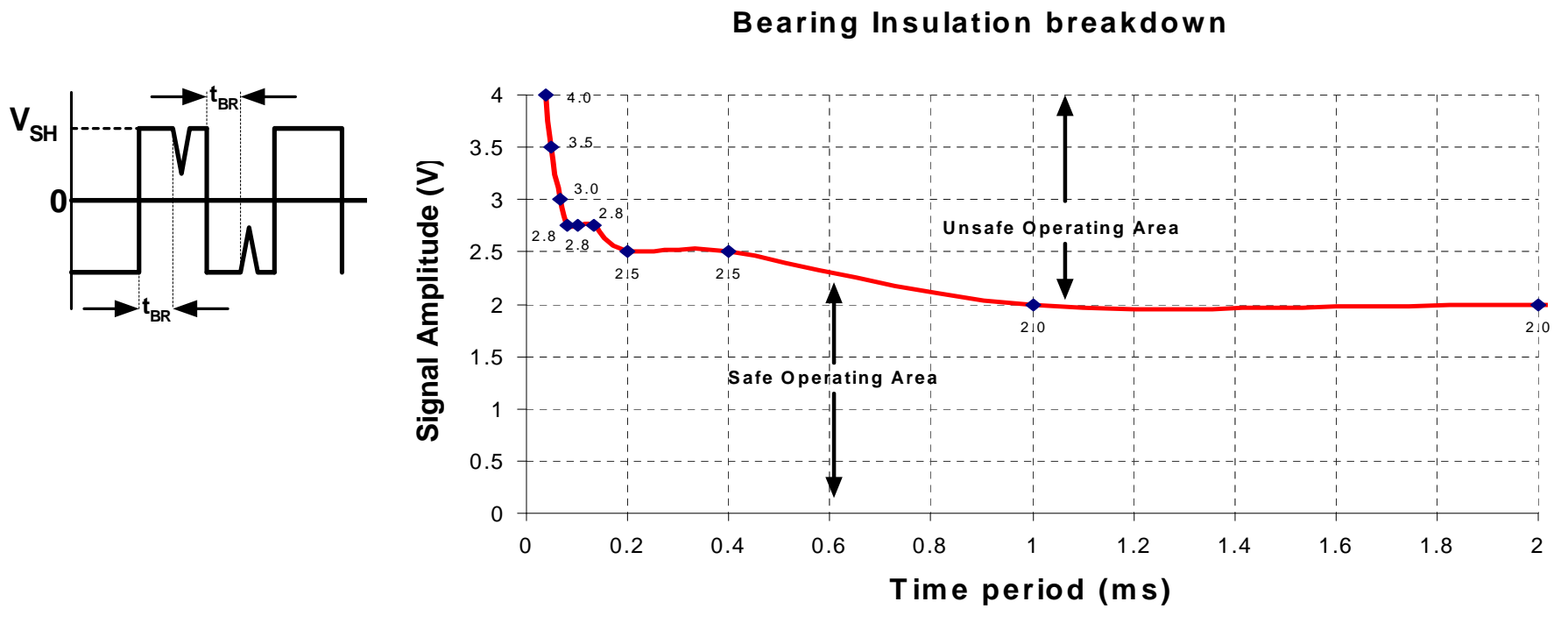


$$I_{brg} = I_{cc} \cdot \frac{1/C_{SF}}{(1/C_{SF}) + (1/C_{SR}) + (1/(C_{RF} + C_{B1} + C_{B2}))}$$

Electrical representation of parasitic capacitances in a motor

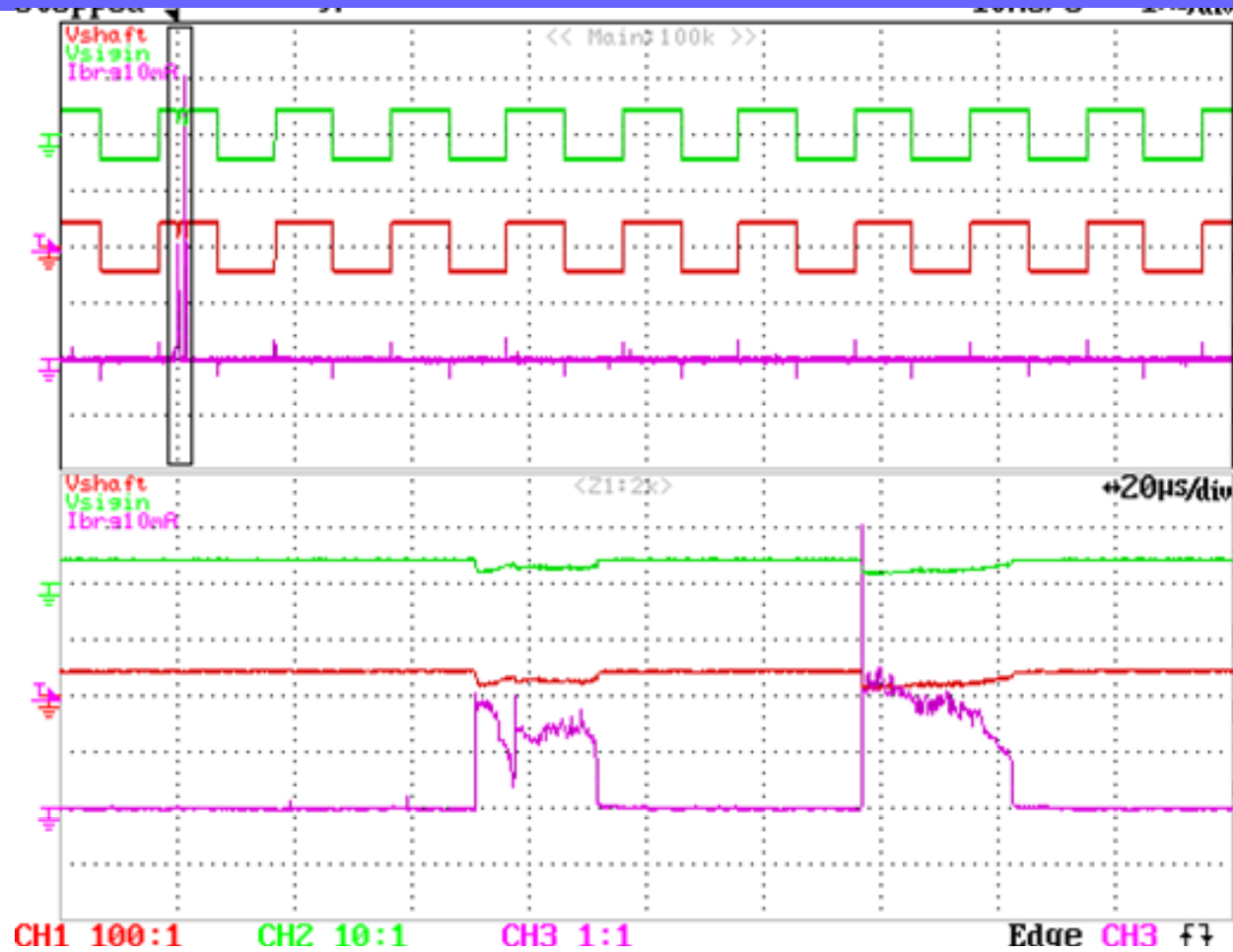
Test 1. Time-Period (Frequency) vs. Shaft voltage (V_{SH})

(Symmetric Rectangular Waveforms of Different Frequencies)



- At higher frequency, breakdown occurs in shorter time for a given shaft voltage. Breakdown voltage is also higher at higher frequency
- At low frequency (180Hz), bearing insulation breaks down at lower shaft voltage – though it takes longer time to breakdown

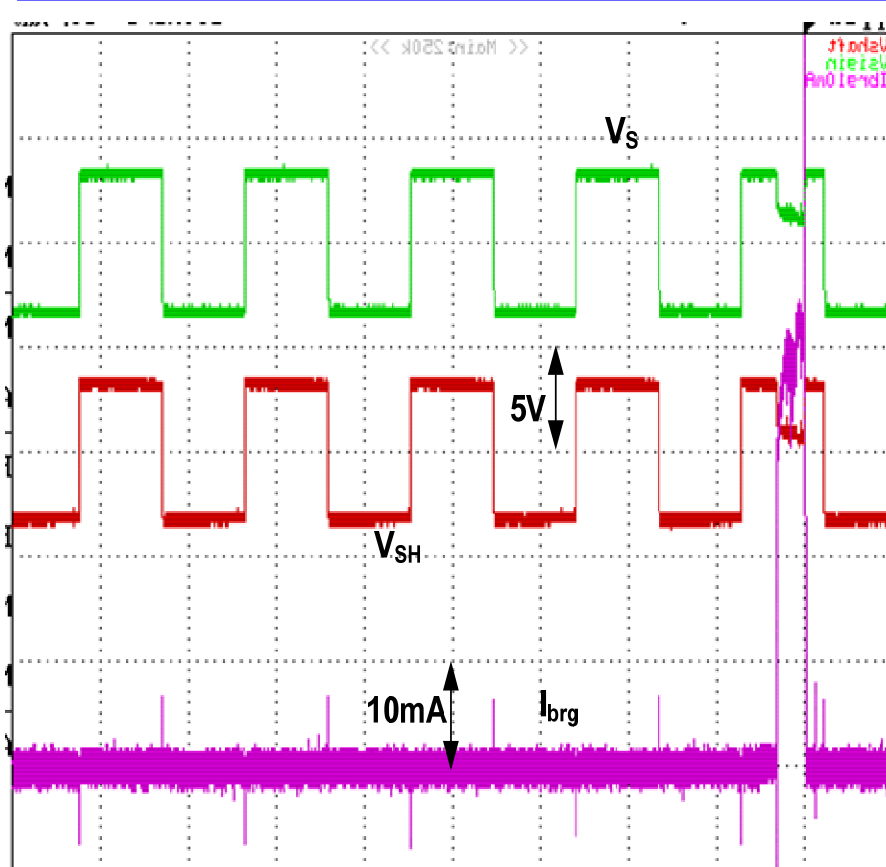
Sample Waveforms for Test 1



Time period= 1.0ms

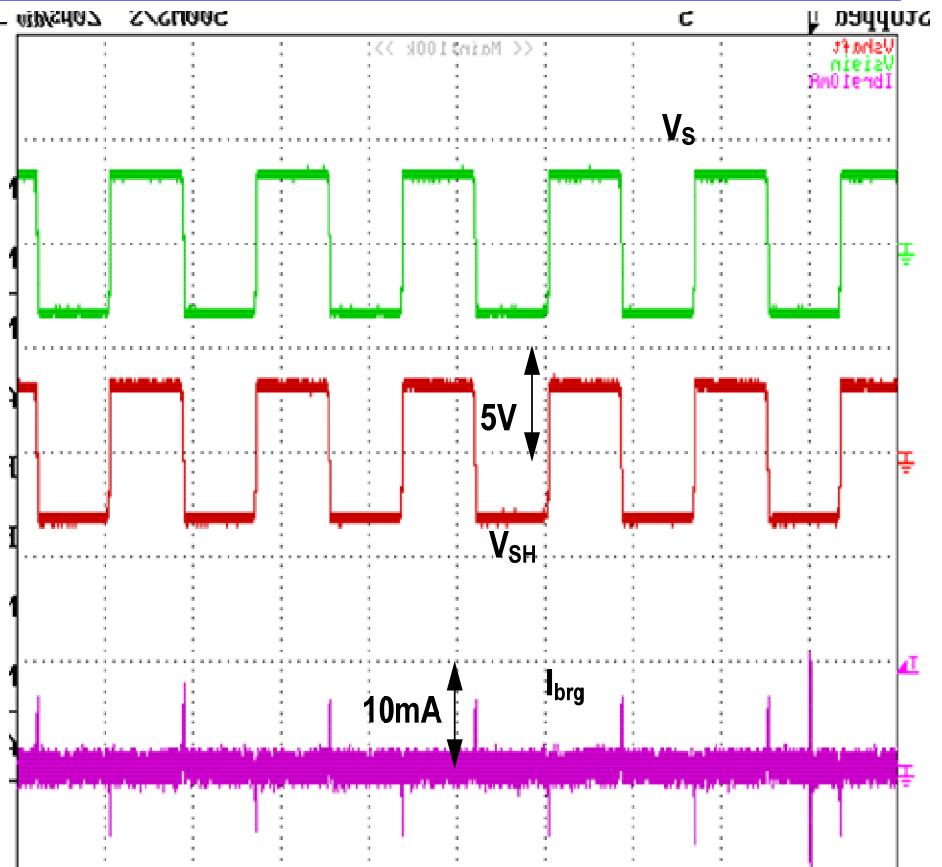
Breakdown occurs at 2.0 Vp-p

Sample Waveforms for Test 1 – Contd.



Time period= 0.1ms

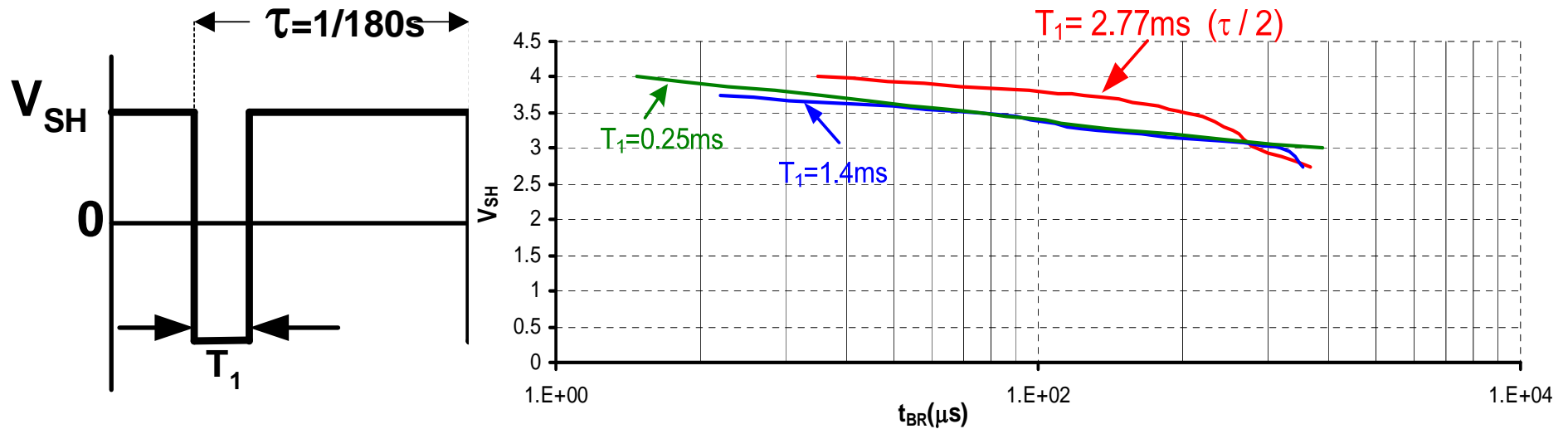
Breakdown occurs at 3.5 Vp-p



Time period= 0.033ms

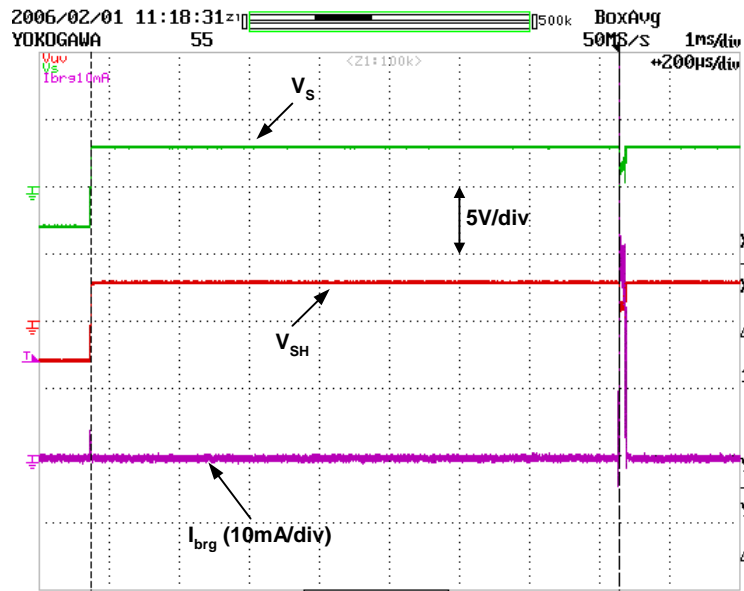
No Breakdown occurs at 3.5 Vp-p

Test 2. Time-to-breakdown (t_{BR}) vs. Shaft voltage (V_{SH}) (180Hz, Asymmetric Rectangular Waveform)

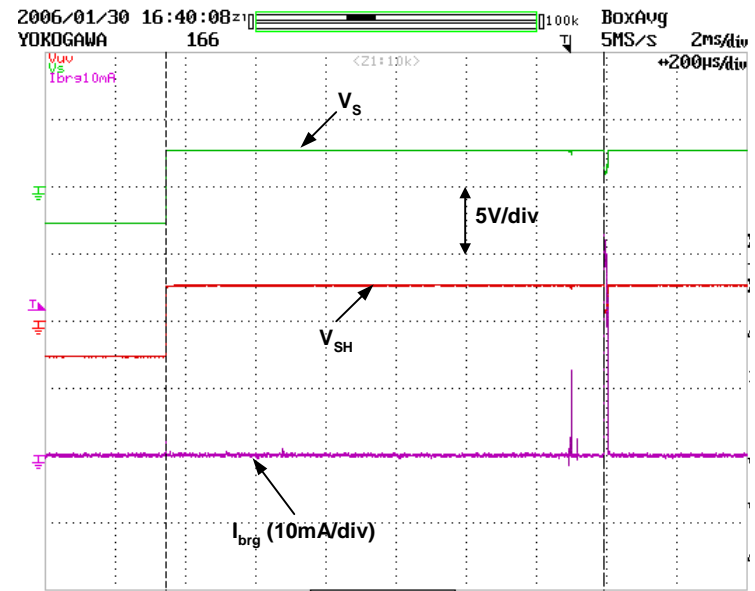


- At low frequency, duration of T_1 does not significantly influence the shaft breakdown voltage.
- However, influence of Asymmetry is not pronounced.

Sample Waveforms for Test 2

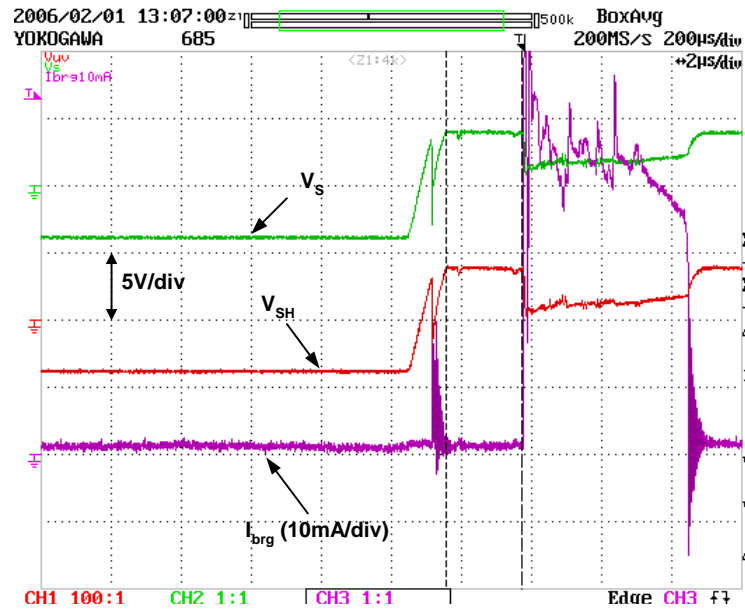


180Hz, $T_1=0.25\text{mS}$
 $t_{BR} = 1.51\text{ms}$ at $V_{SH}=\pm 3\text{V}$

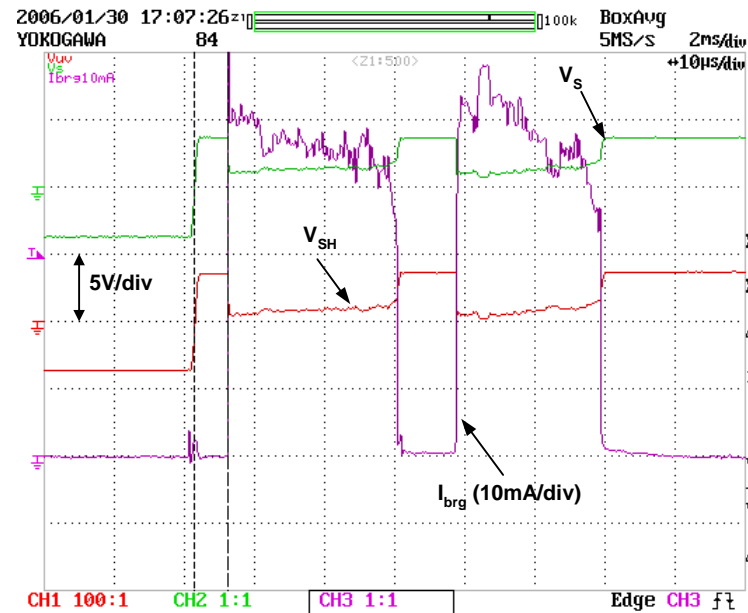


180Hz, $T_1=1.4\text{mS}$
 $t_{BR} = 1.24\text{ms}$ at $V_{SH}=\pm 2.75\text{V}$

Sample Waveforms for Test 2 – Contd.

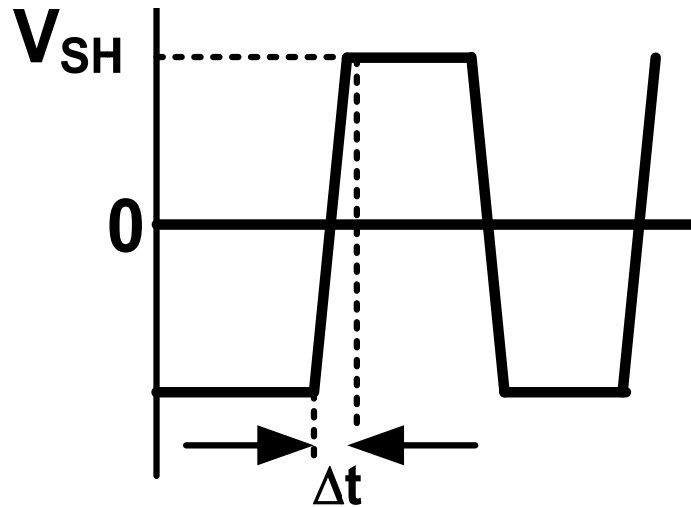


180Hz, $T_1=0.25\text{mS}$
 $t_{BR} = 2.15\mu\text{s}$ at $V_{SH}=\pm 4\text{V}$



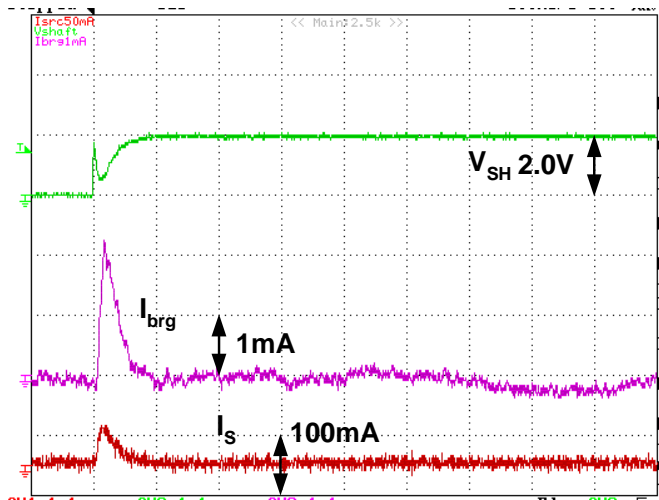
180Hz, $T_1=1.4\text{mS}$
 $t_{BR} = 4.8\mu\text{s}$ at $V_{SH}=\pm 3.75\text{V}$

Test 3. Bearing insulation break down versus dv/dt of shaft voltage

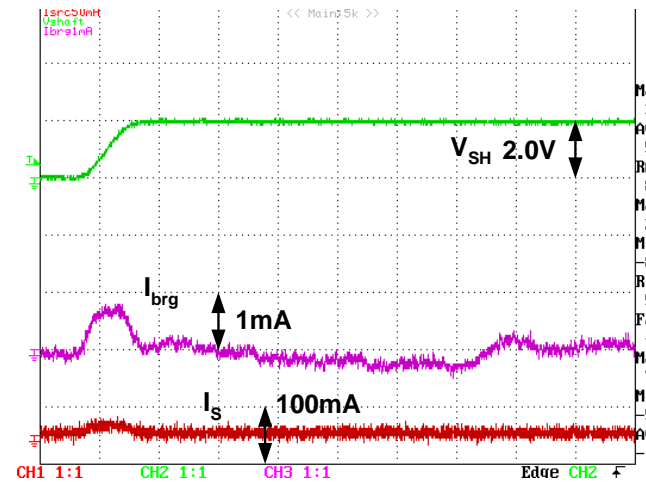


- Bearing film insulation breakdown phenomenon is observed to be independent of the dv/dt of the applied voltage.
- Low shaft voltage, even with high dv/dt , does not cause the bearing film insulation to breakdown.
- High shaft voltage, even with low dv/dt , causes the bearing film insulation to breakdown easily.
- When the dv/dt of the externally injected square voltage is changed from 4ns to 400ns or greater, the charging current into the bearing does not reduce by the same factor, as does the dv/dt . This shows that the charging bearing current is also a function of the dc component of the applied voltage.

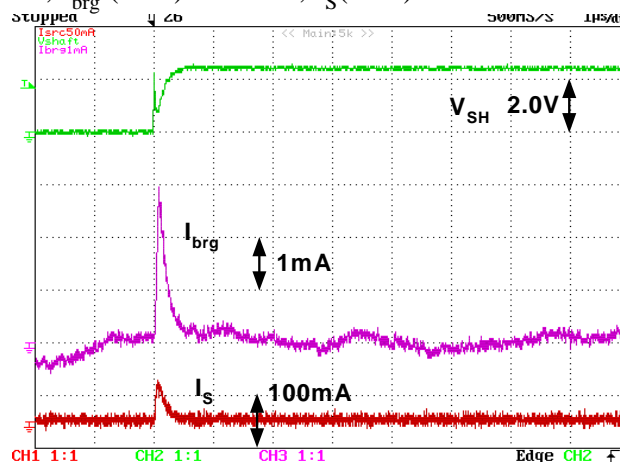
Tests: Bearing insulation break down versus dv/dt of shaft voltage



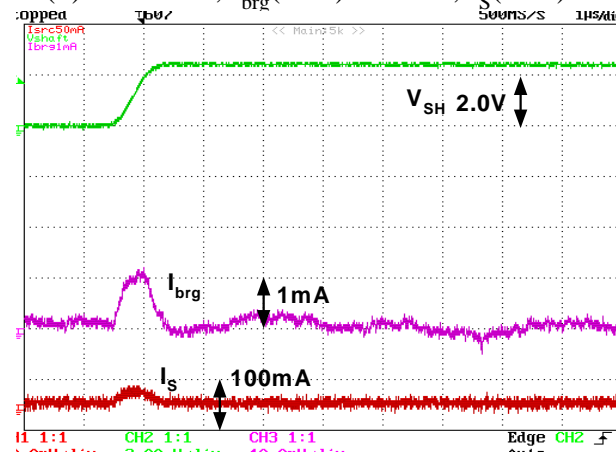
(a) 2V/4ns, $I_{brg}(\max) = 2.5mA$, $I_S(\max) = 67mA$



(b) 2V/556ns, $I_{brg}(\max) = 0.8mA$, $I_S(\max) = 33.3mA$

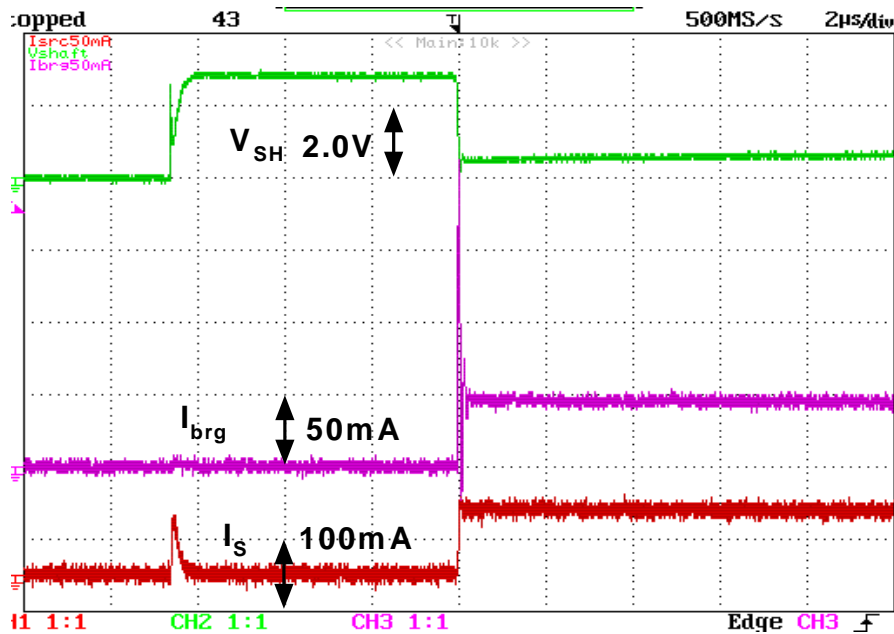


(c) 2.5V/4ns, $I_{brg}(\max) = 2.95mA$, $I_S(\max) = 79mA$

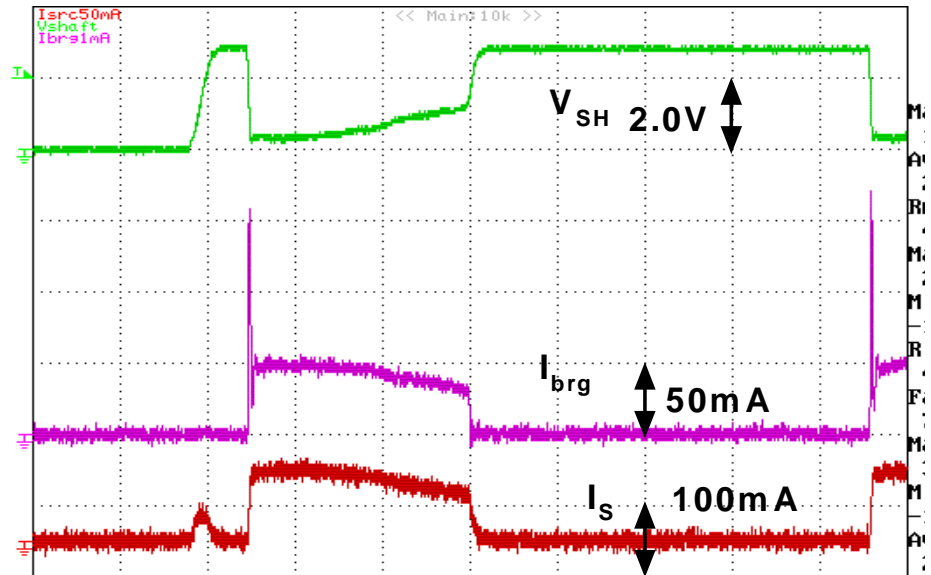


(d) 2.5V/534ns, $I_{brg}(\max) = 1.2mA$, $I_S(\max) = 37mA$

Tests: Bearing insulation break down versus dv/dt of shaft voltage

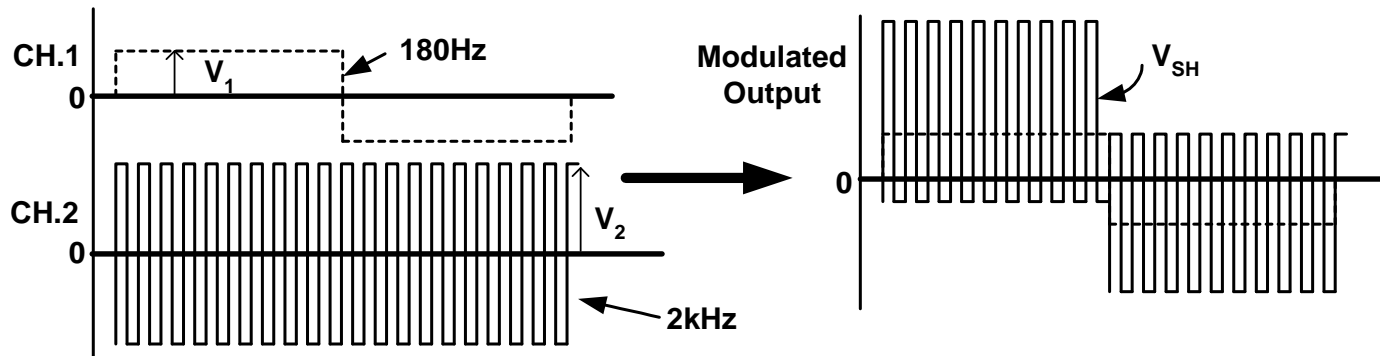
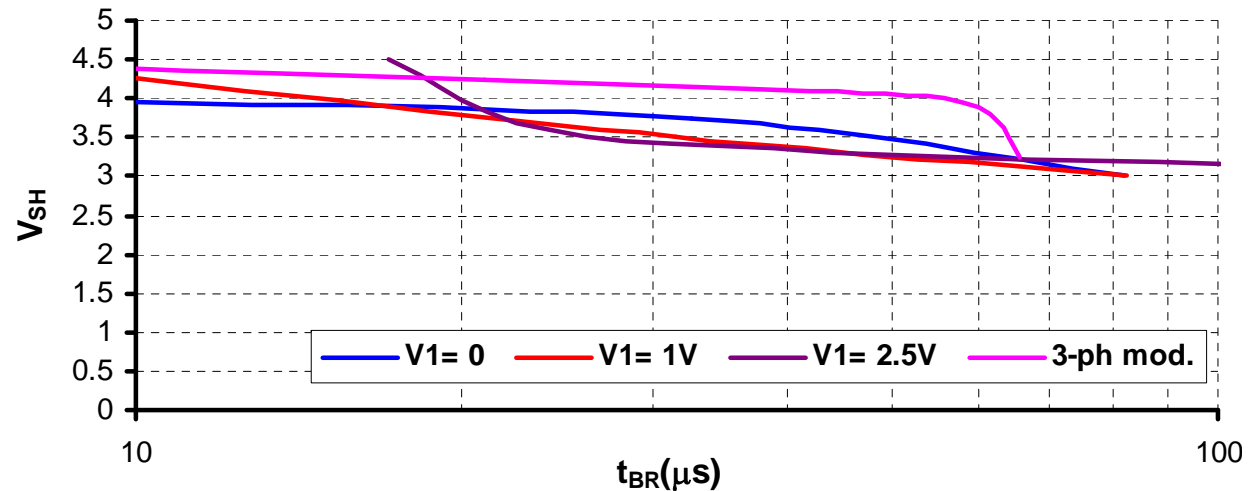
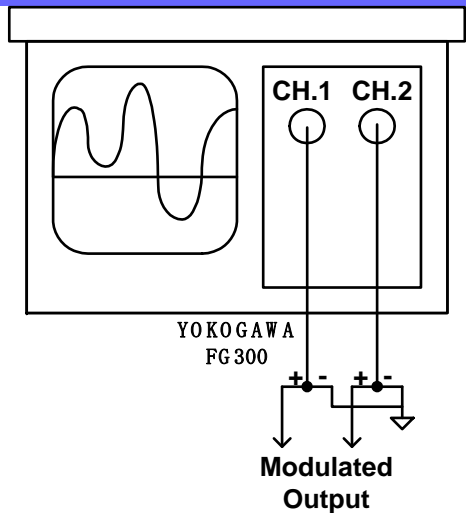


(e) Breakdown at 3V/4ns, $I_{brg}(\max) = 212.5\text{mA}$,
 $I_s(\max) = 56.25\text{mA}$



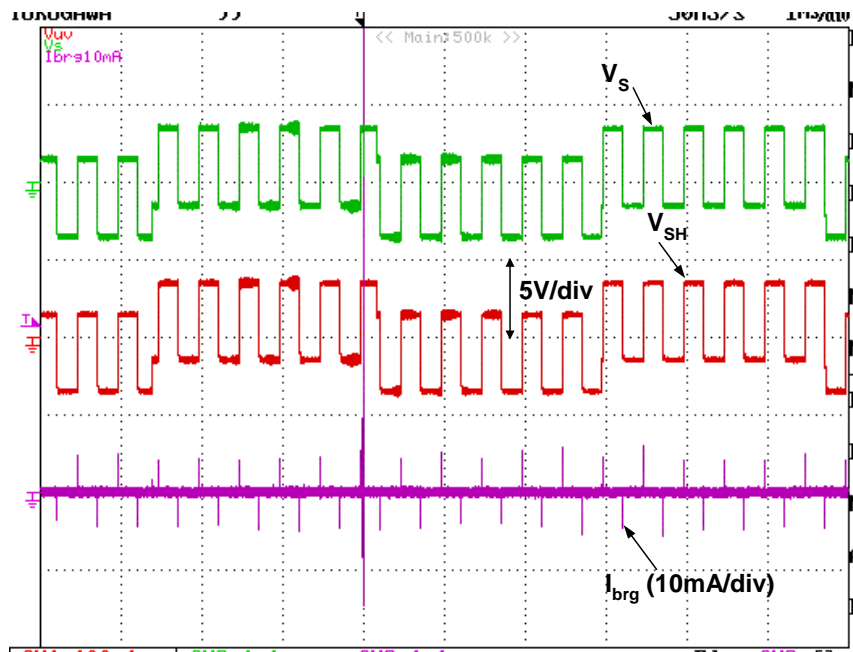
(f) Breakdown at 3V/404ns, $I_{brg}(\max) = 170\text{mA}$,
 $I_s(\max) = 58\text{mA}$

Test 4. Time-to-breakdown (t_{BR}) vs. Shaft voltage (V_{SH}) (2kHz Rectangular Waveform Modulated with 180Hz Signal)

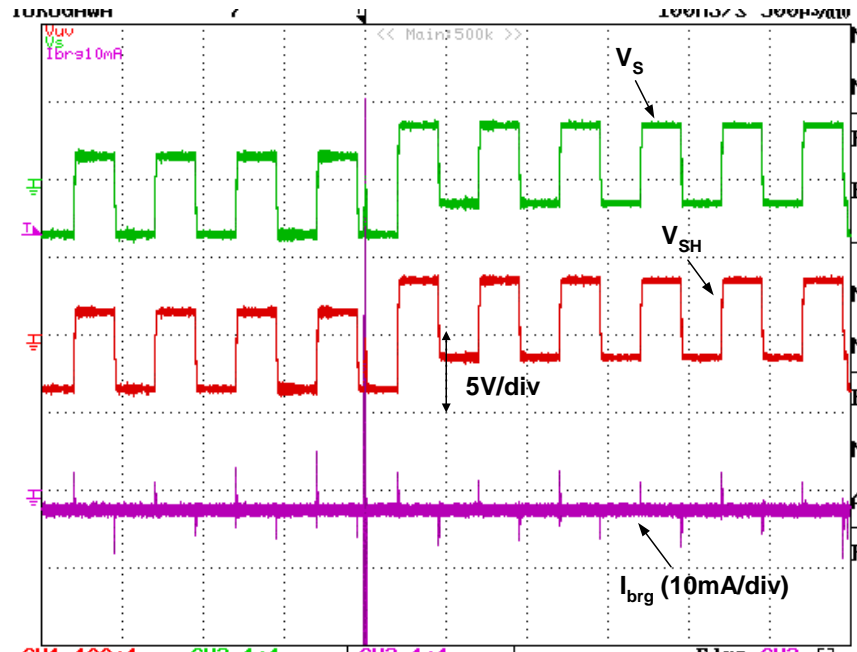


- The modulated waveform emulates shaft voltage associated with 2-Phase modulation.
- No orderly effect of modulation to breakdown time was observed.

Sample Waveforms for Test 4

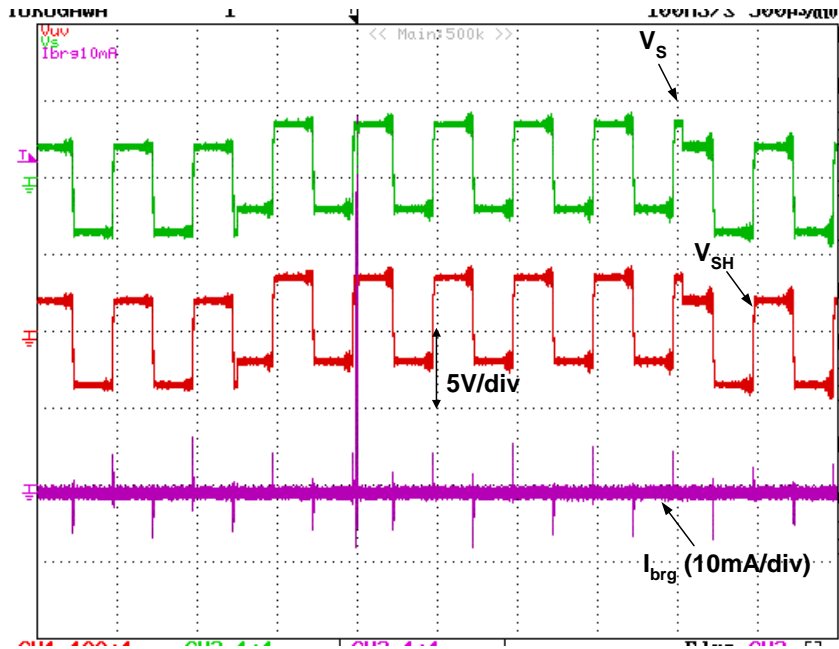


$V_1 = 1V$
 $t_{BR} = 31.5\mu s$ at $7.0 V_{p-p}$

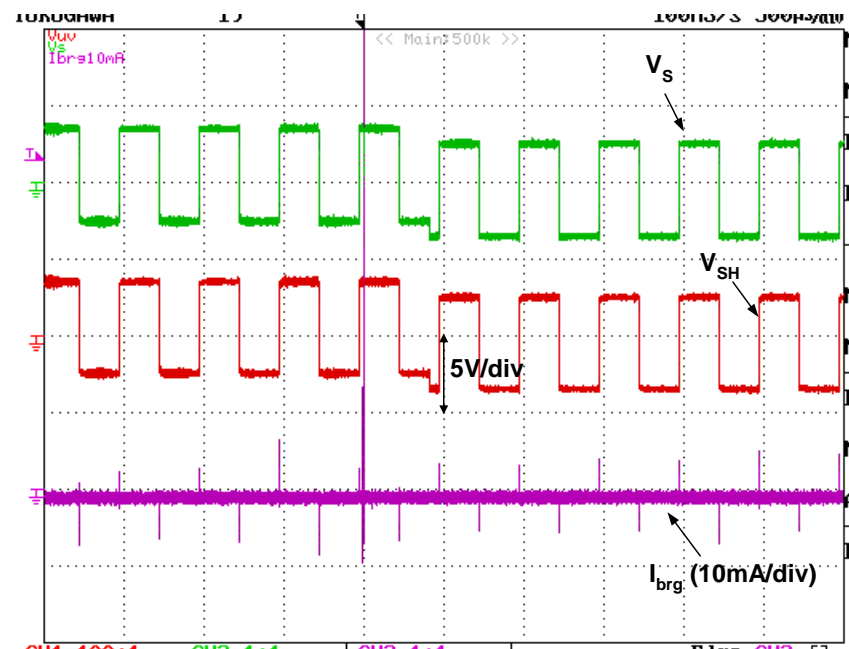


$V_1 = 1.5V$
 $t_{BR} = 40.4\mu s$ at $7.0 V_{p-p}$

Sample Waveforms for Test 4

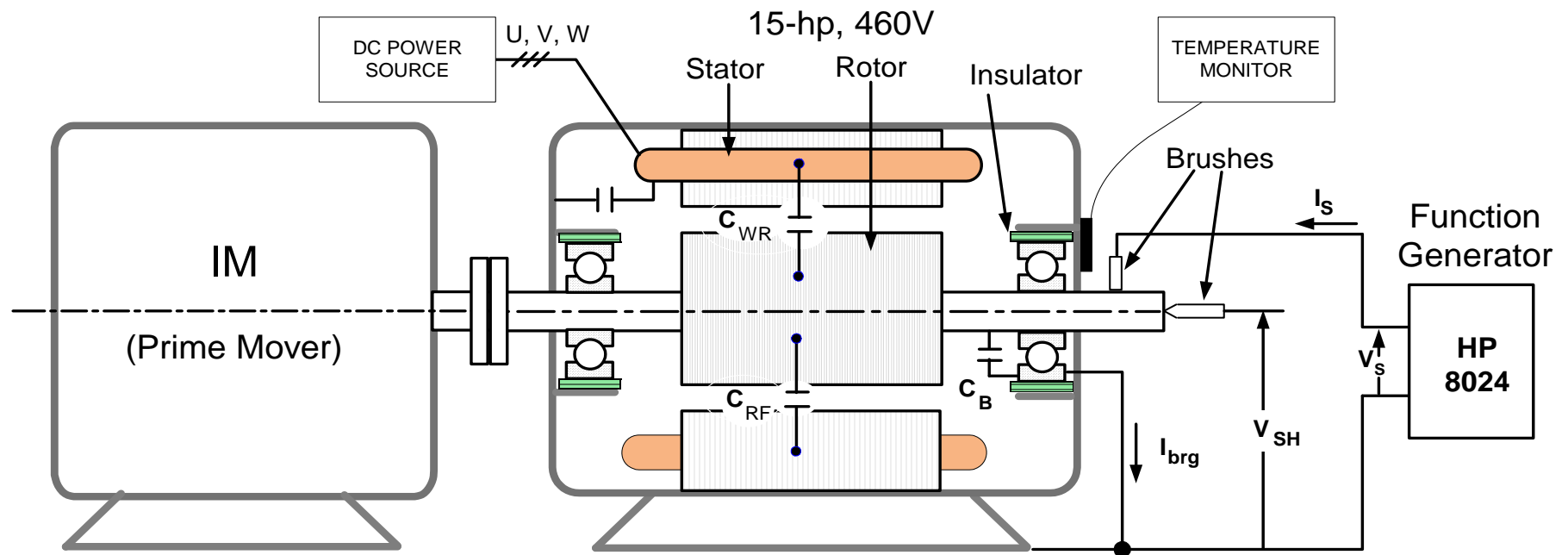


$V_1 = 2V$
 $t_{BR} = 21.8\mu s$ at $7.0 V_{p-p}$



$V_1 = 2.5V$
 $t_{BR} = 26.1\mu s$ at $7.0 V_{p-p}$

Effect of Temperature



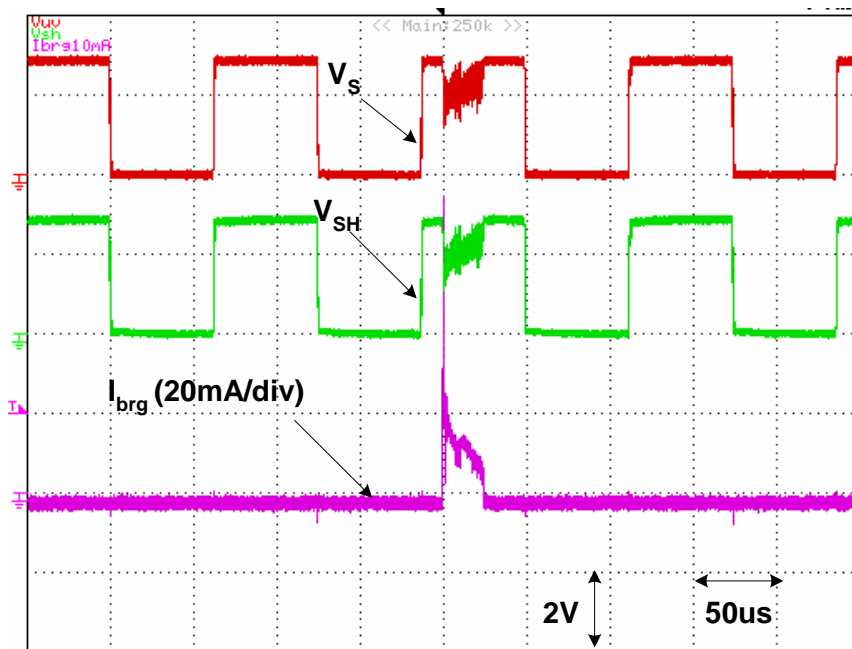
J-Type Thermocouple used

External signal was injected at shaft

Motor was heated using DC injection

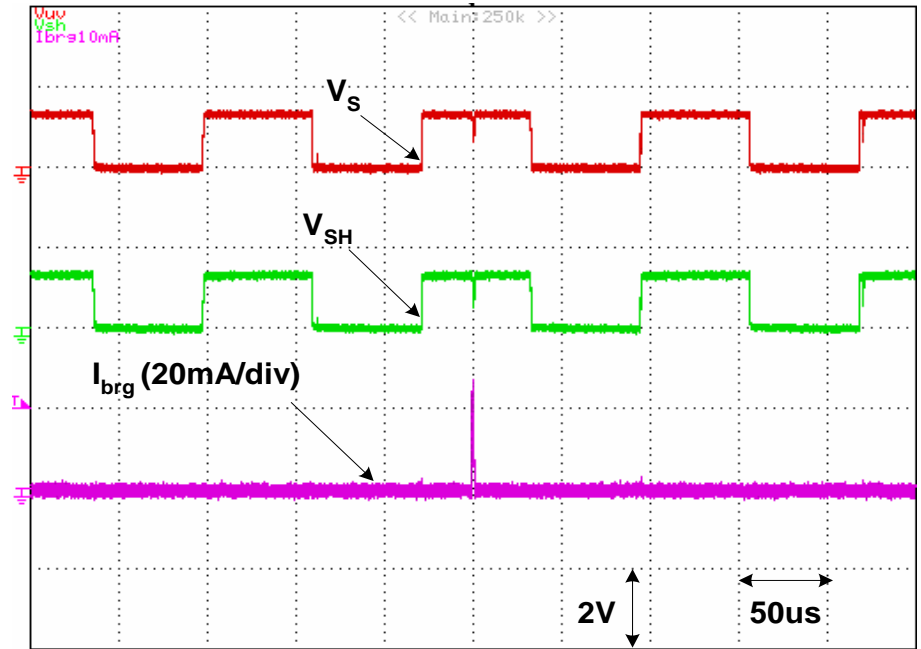
Breakdown voltage as a function of Temperature was studied

Sample Waveforms for Temperature Test



Temperature = 25.6 deg. C

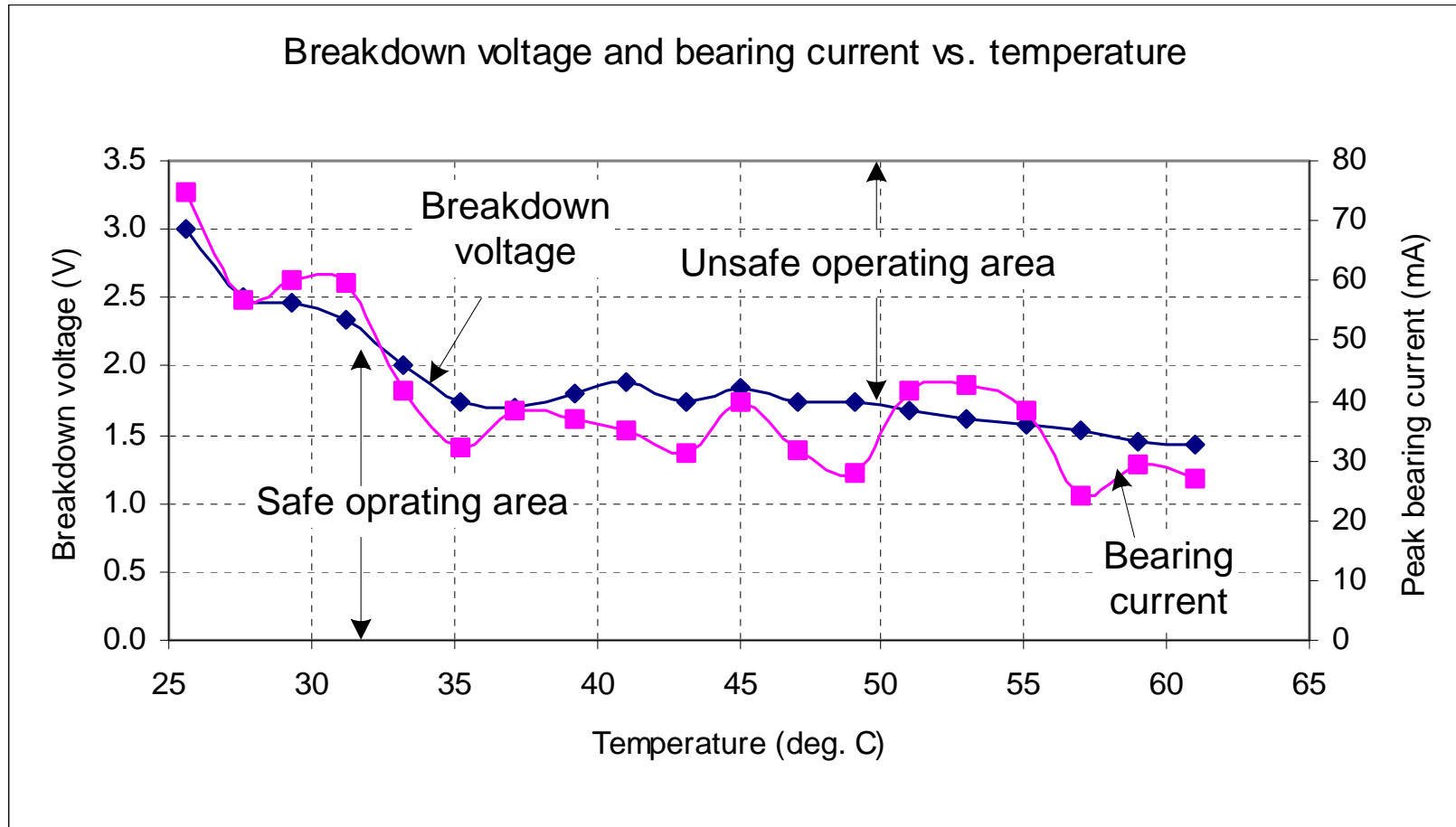
Breakdown Voltage = 3V



Temperature = 61 deg. C

Breakdown Voltage = 1.42V

Breakdown Voltage Versus Temperature



4. Key Observations

- At higher frequency, breakdown occurs in shorter time; At low frequency (180Hz) break down occurs at lower shaft voltage.
- Asymmetric Waveform with shorter negative period shows lower breakdown voltage.
However, influence of asymmetry is not pronounced.
- dv/dt of waveform does NOT directly influence the breakdown of bearing phenomenon – it may be responsible to increase the temperature of the bearing and hence accelerate the breakdown
- Modulated waveform showed no definite correlation with breakdown time.
- Higher temperature reduces shaft breakdown voltage significantly.

5. Mitigation Techniques

- Shaft Brush.
- Faraday Shield.
- Common Mode Filters
- 3-Level Inverters.

6. Shaft Brush

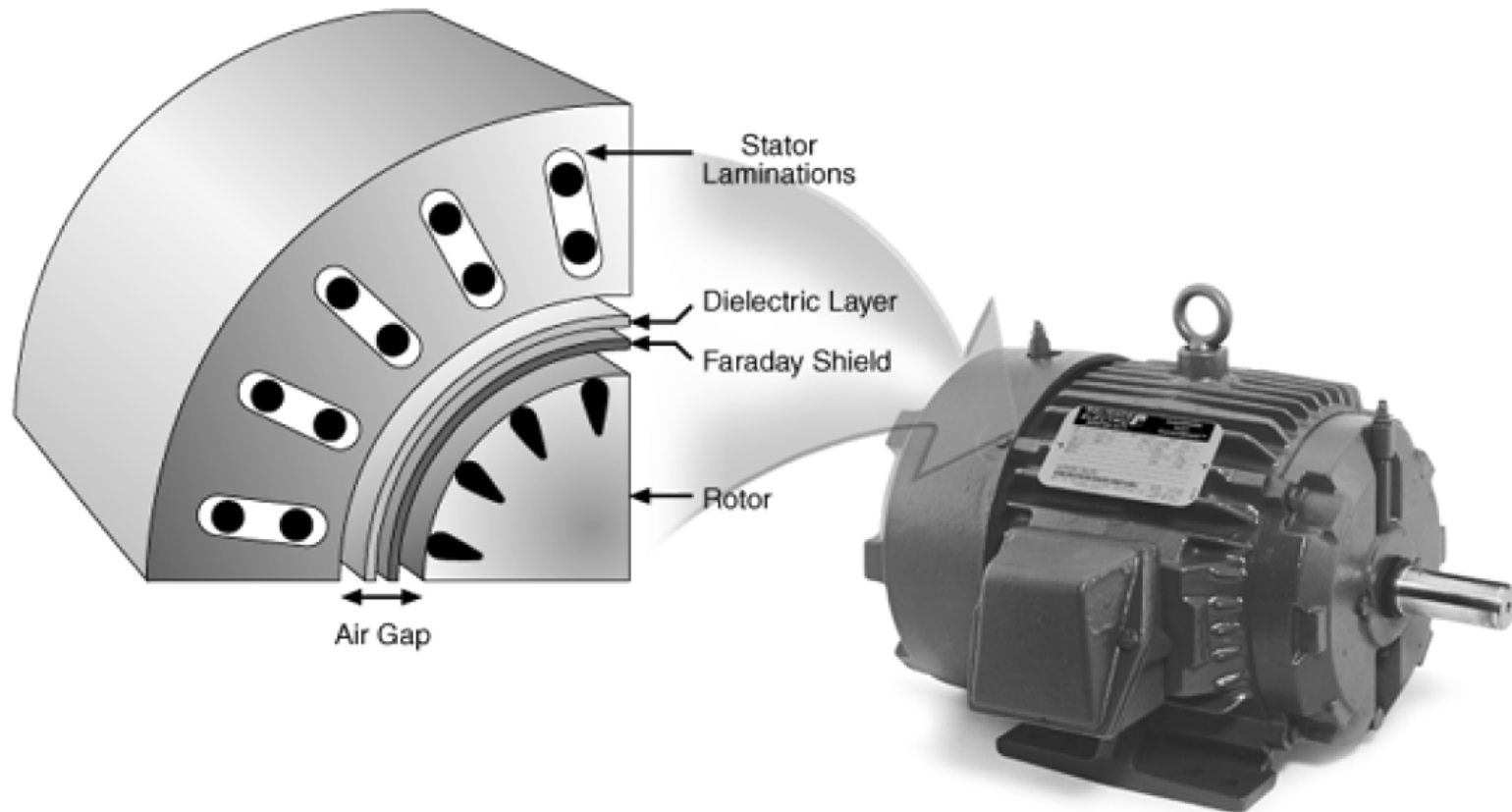
BRUSH-HOLDER KIT FOR GROUNDING OF ELECTRIC MOTORS BEARINGS

(APPLIED WITH FREQUENCY INVERTER)



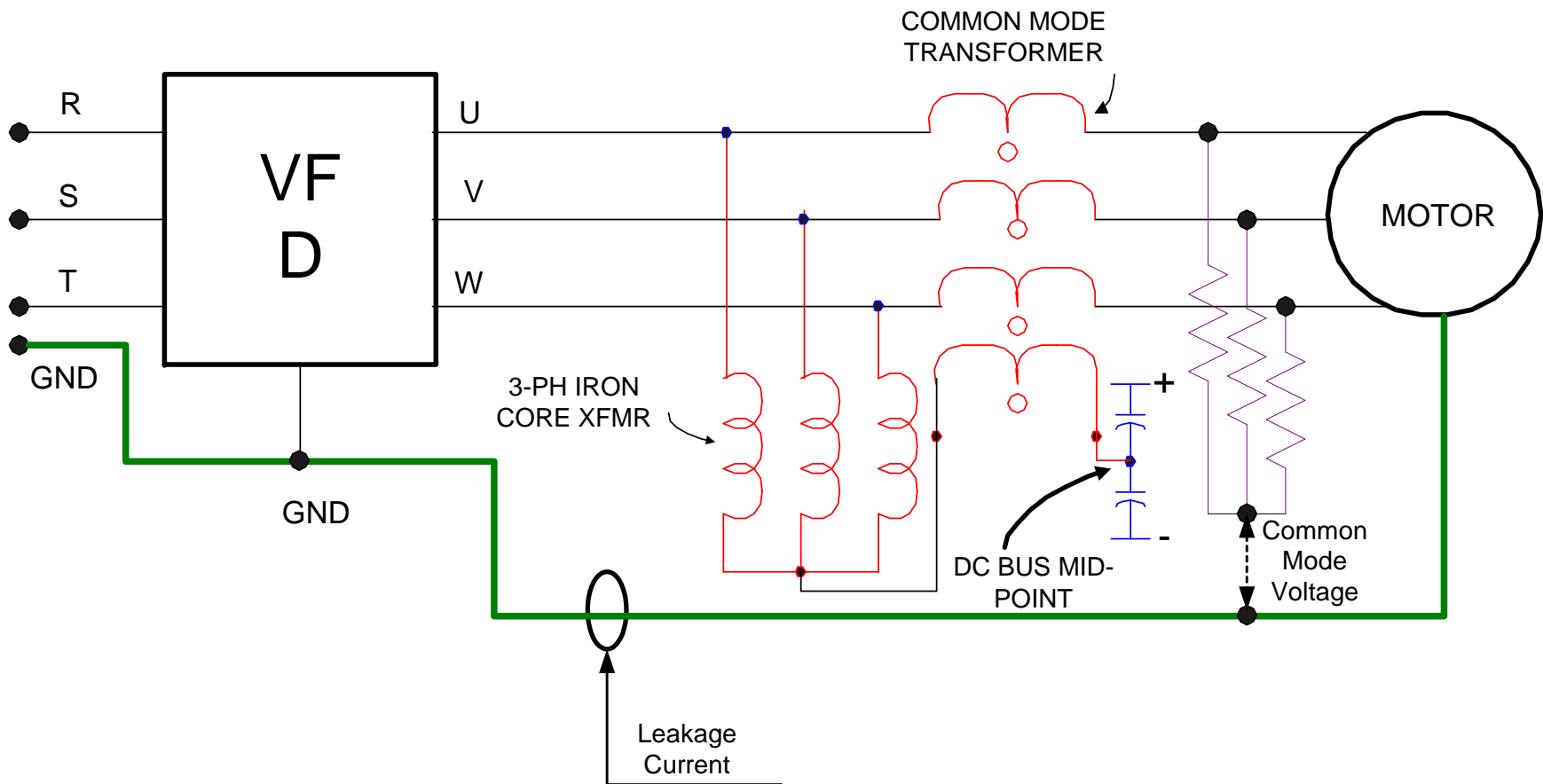
- Simple and effective
- Needs maintenance, typically after 20,000hrs of operation
- Metallic dust in air is not suitable for clean room applications

7. Faraday Shield

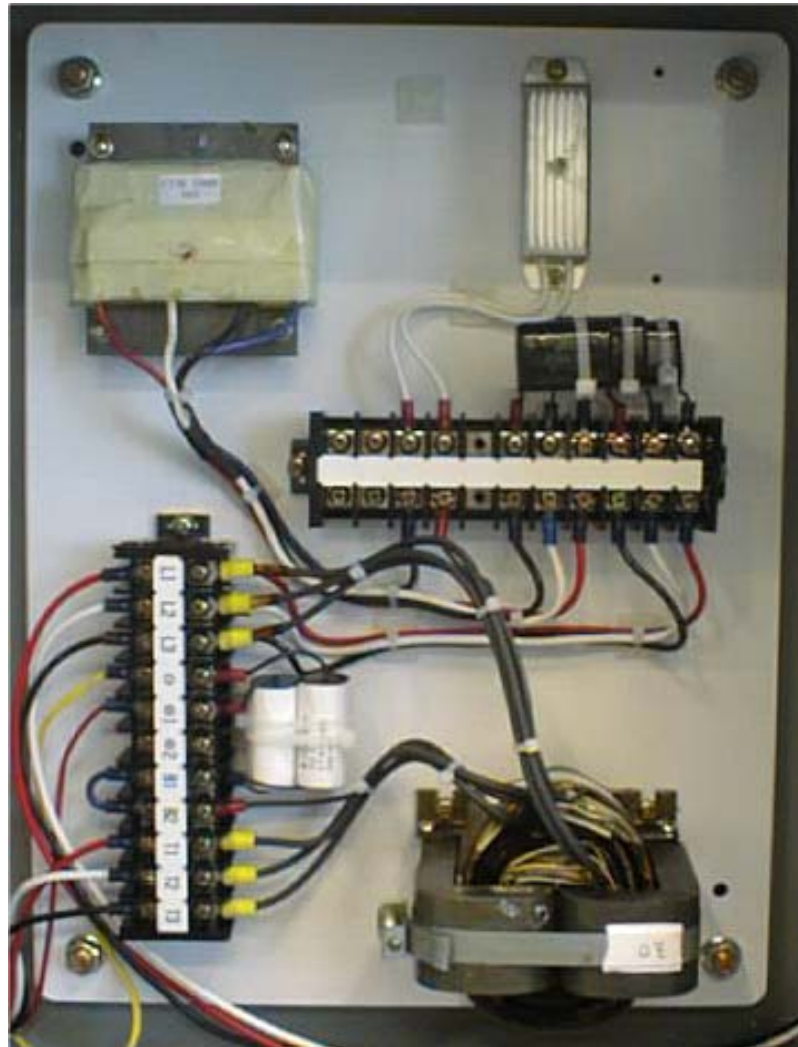


- Quite effective
- Needs to be inserted during manufacturing of motor
- Expensive and causes low frequency power loss

8. Common Mode Voltage Cancellation Circuit



8b. Photo of Common Mode Filter

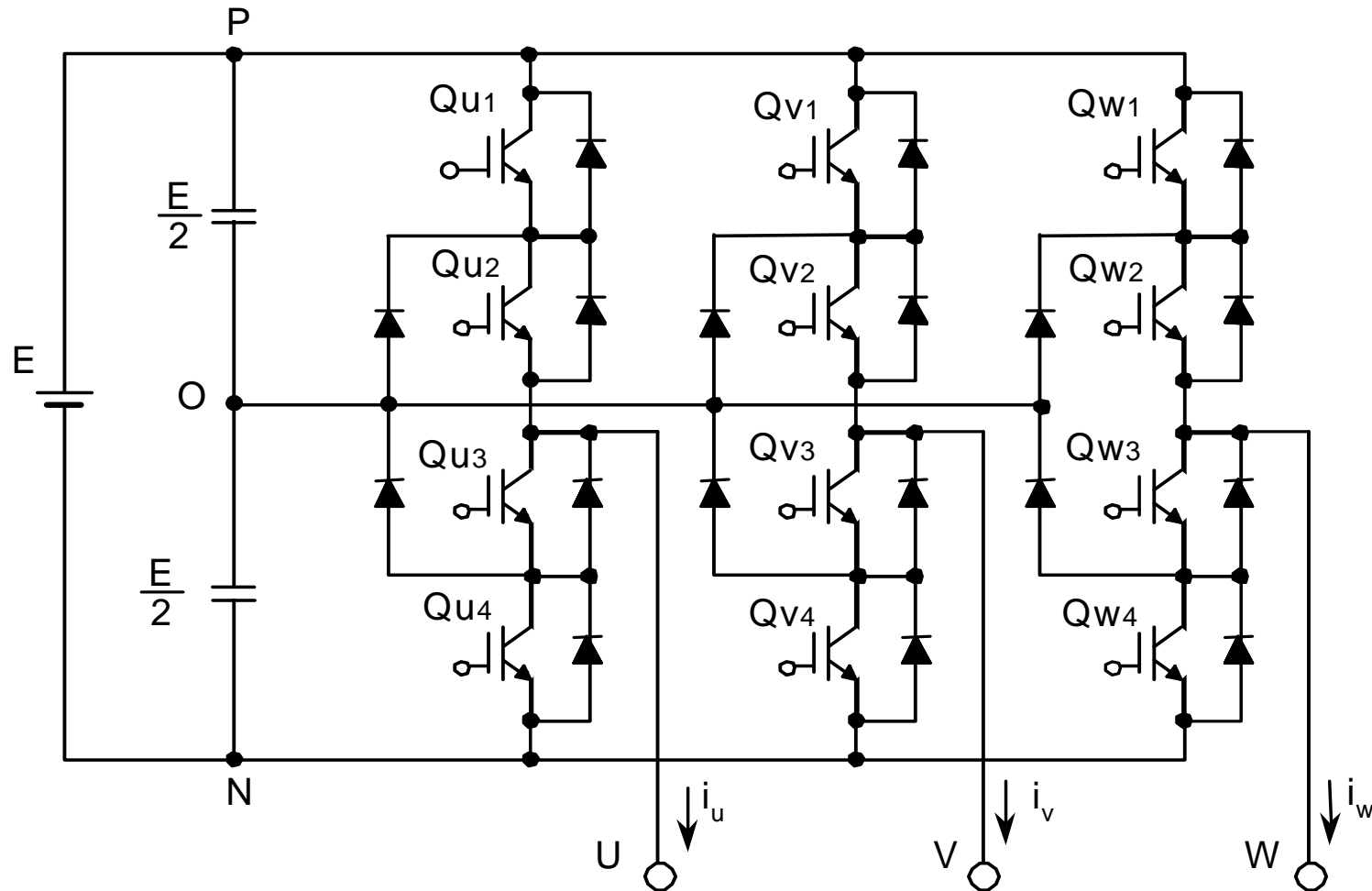


9. NPC Three-Level Inverter

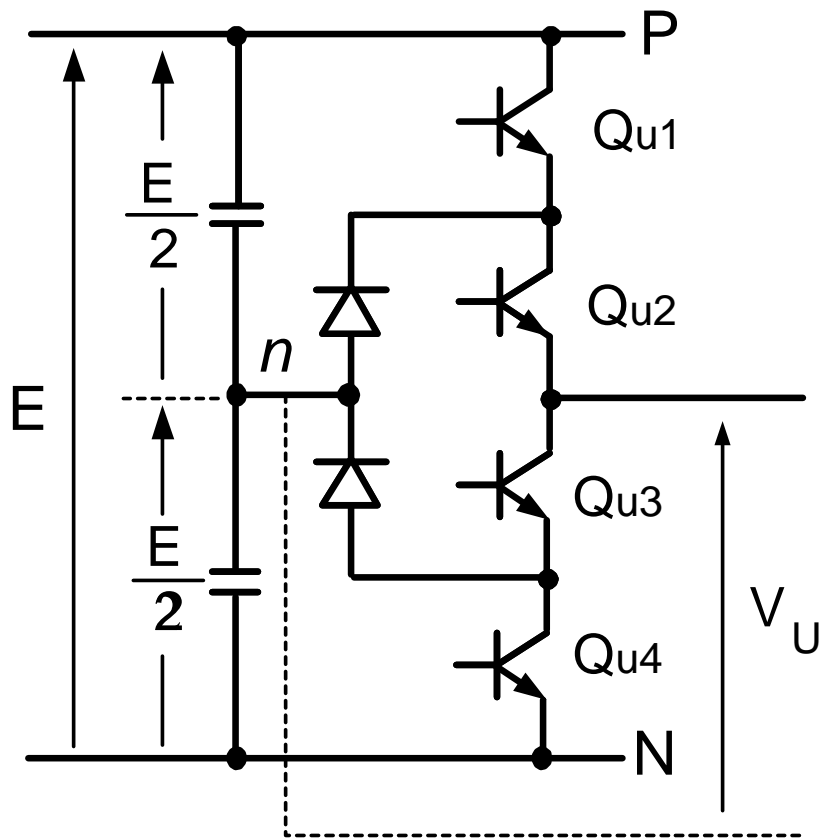
- Common Issues of Voltage Source PWM Inverters:
 - **Surge voltages at motor terminals.**
 - **Leakage current**
 - **Shaft voltage and bearing current**
(possible bearing failures)

Three-level topology addresses the above issues in a cost effective manner.

9a. 3-Level Topology

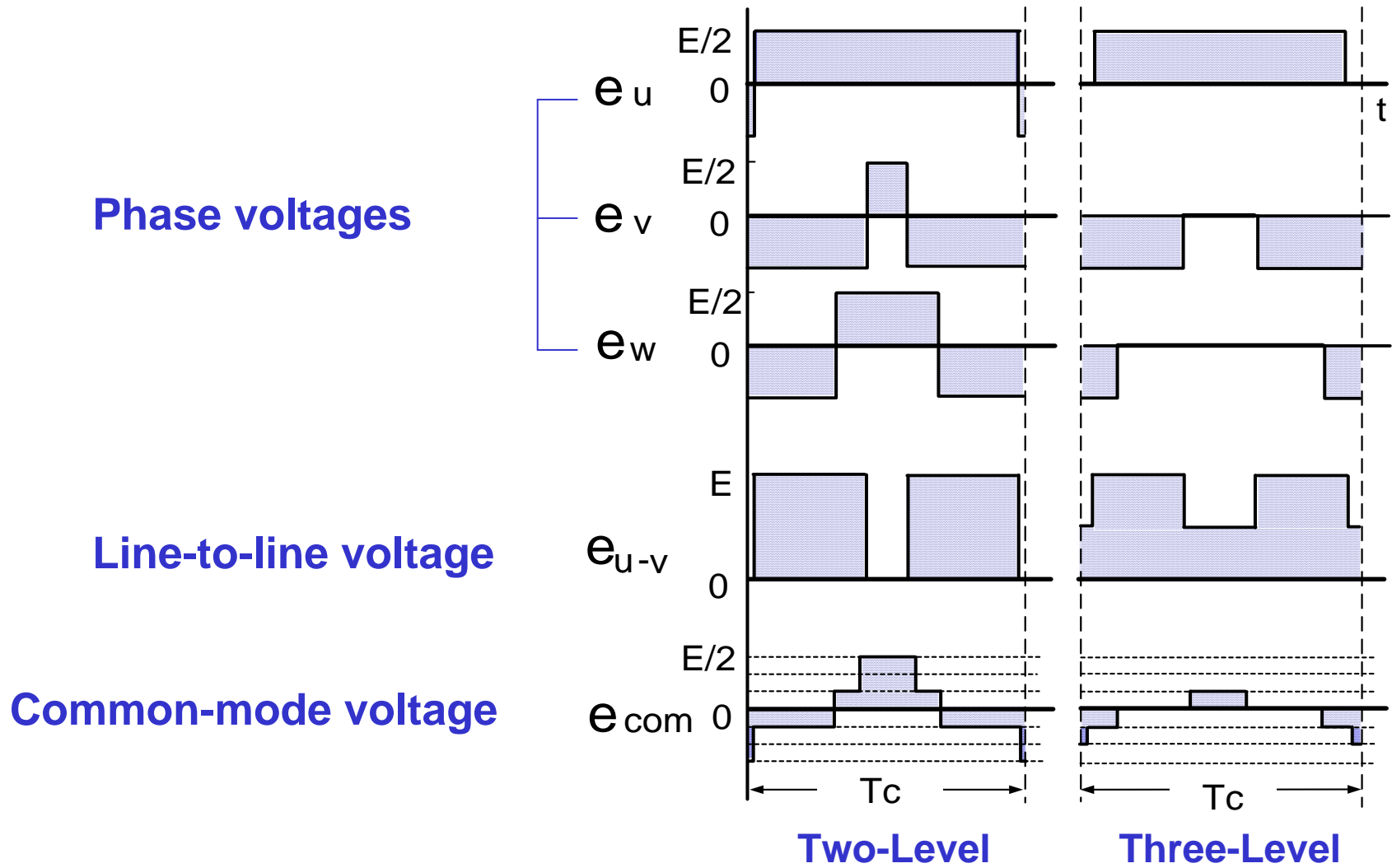


9b. Switching States and Output Voltage



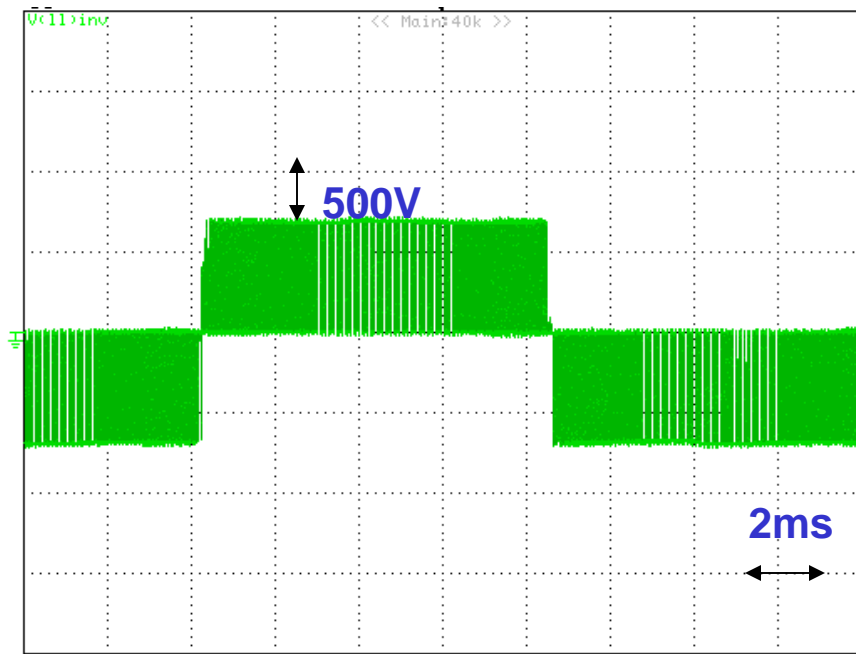
Qu_1	Qu_2	Qu_3	Qu_4	V_u
ON	ON	OFF	OFF	$+E/2$
OFF	OFF	ON	ON	$-E/2$
OFF	ON	ON	OFF	0

9c. Output Voltage Waveforms

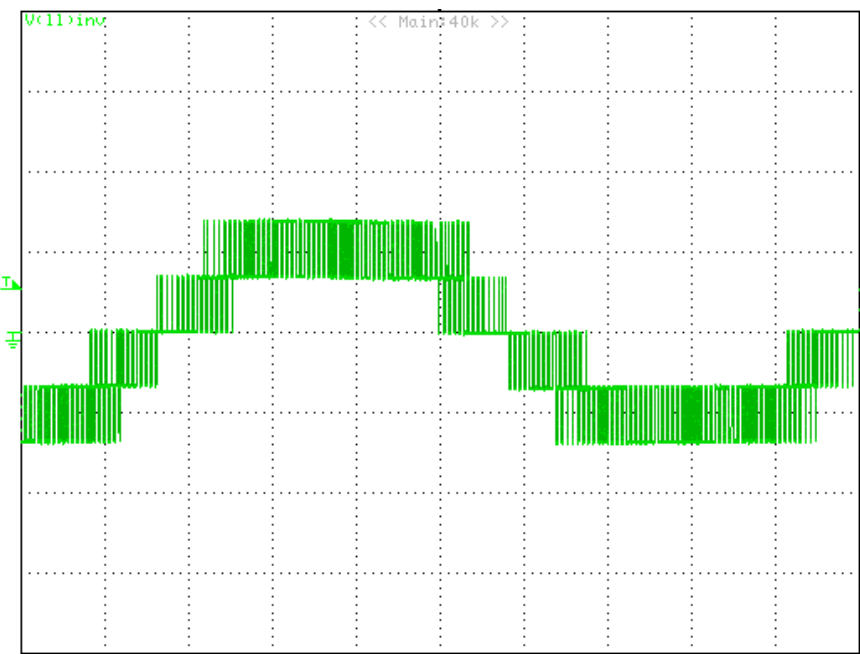


10. Test Results

(460V, 7.5 kW motor drive system)

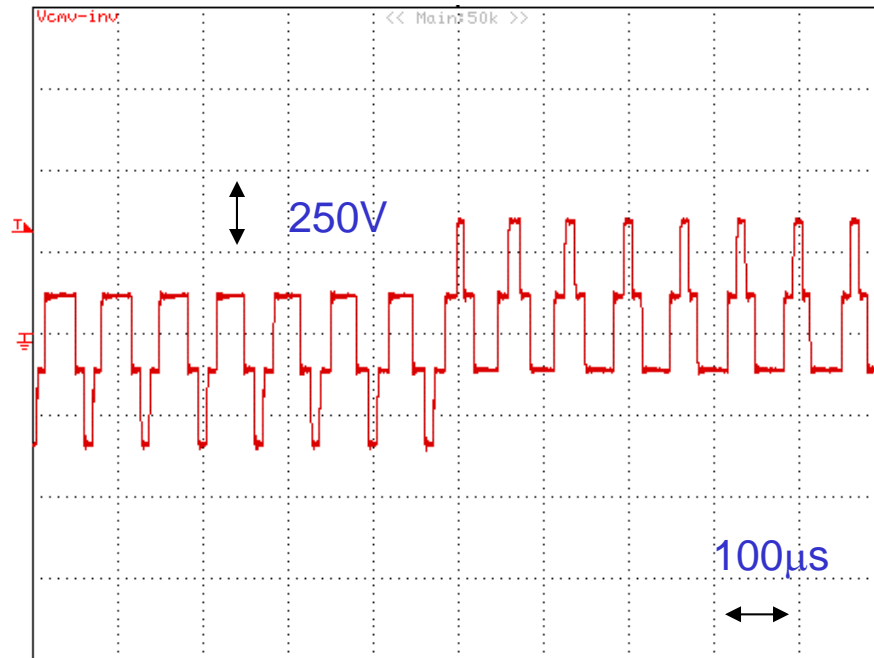


Two-Level Inverter

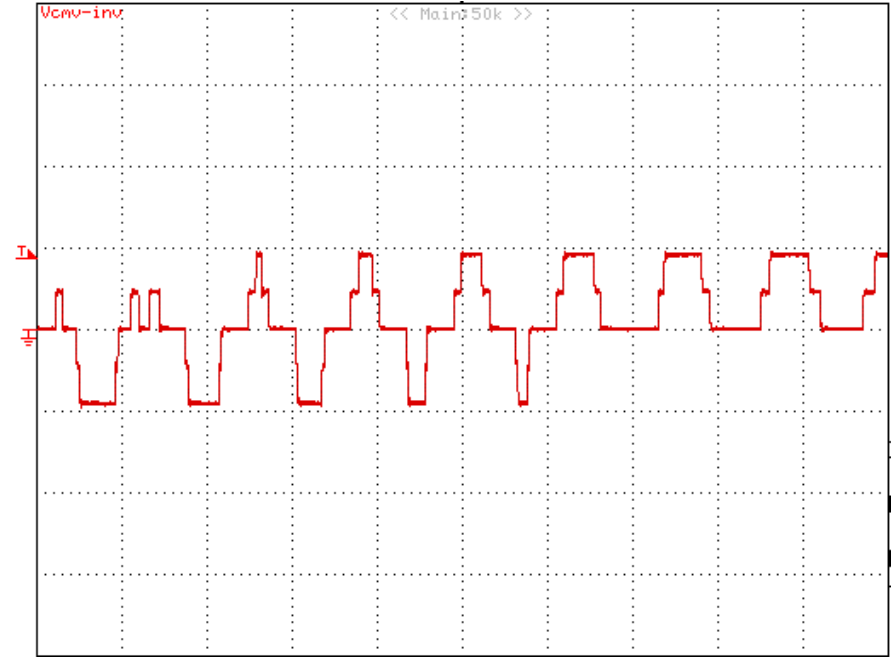


Three-Level Inverter

10a. Measured Common-Mode Voltages

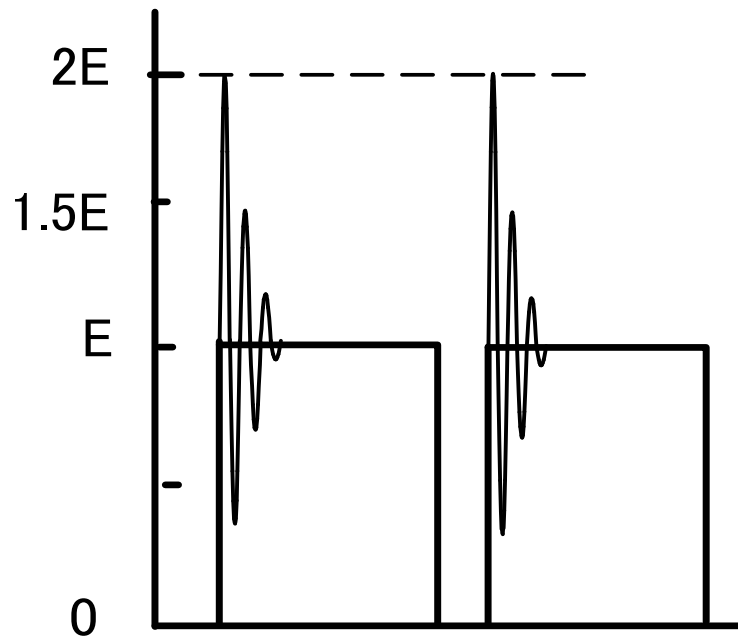


Two-Level Inverter

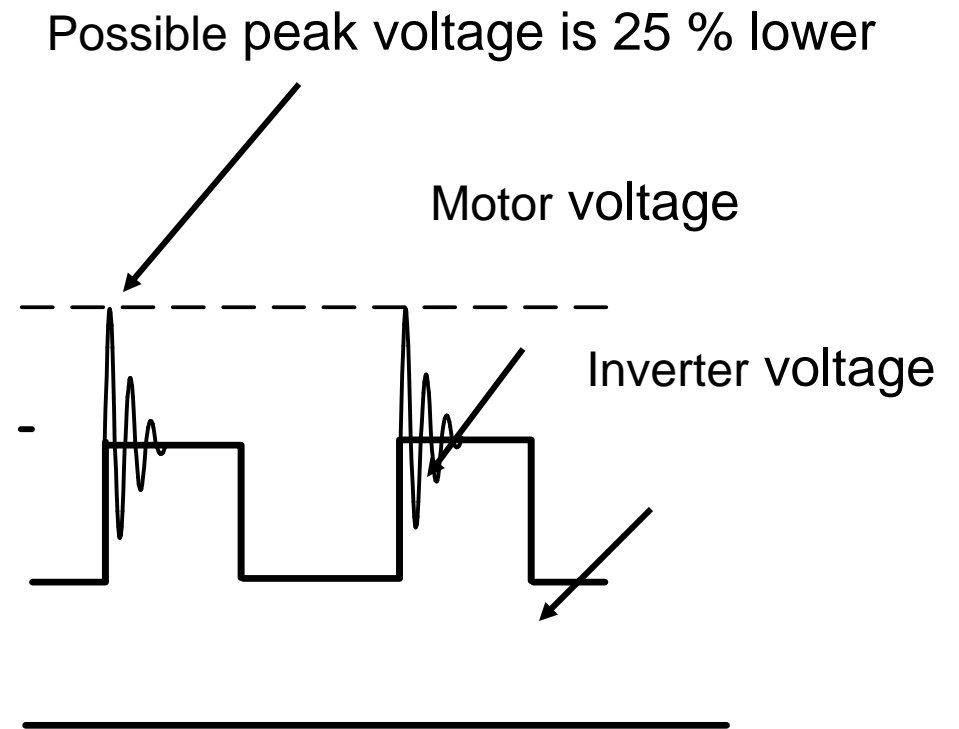


Three-Level Inverter

10c. Voltage Overshoot at Motor Terminals



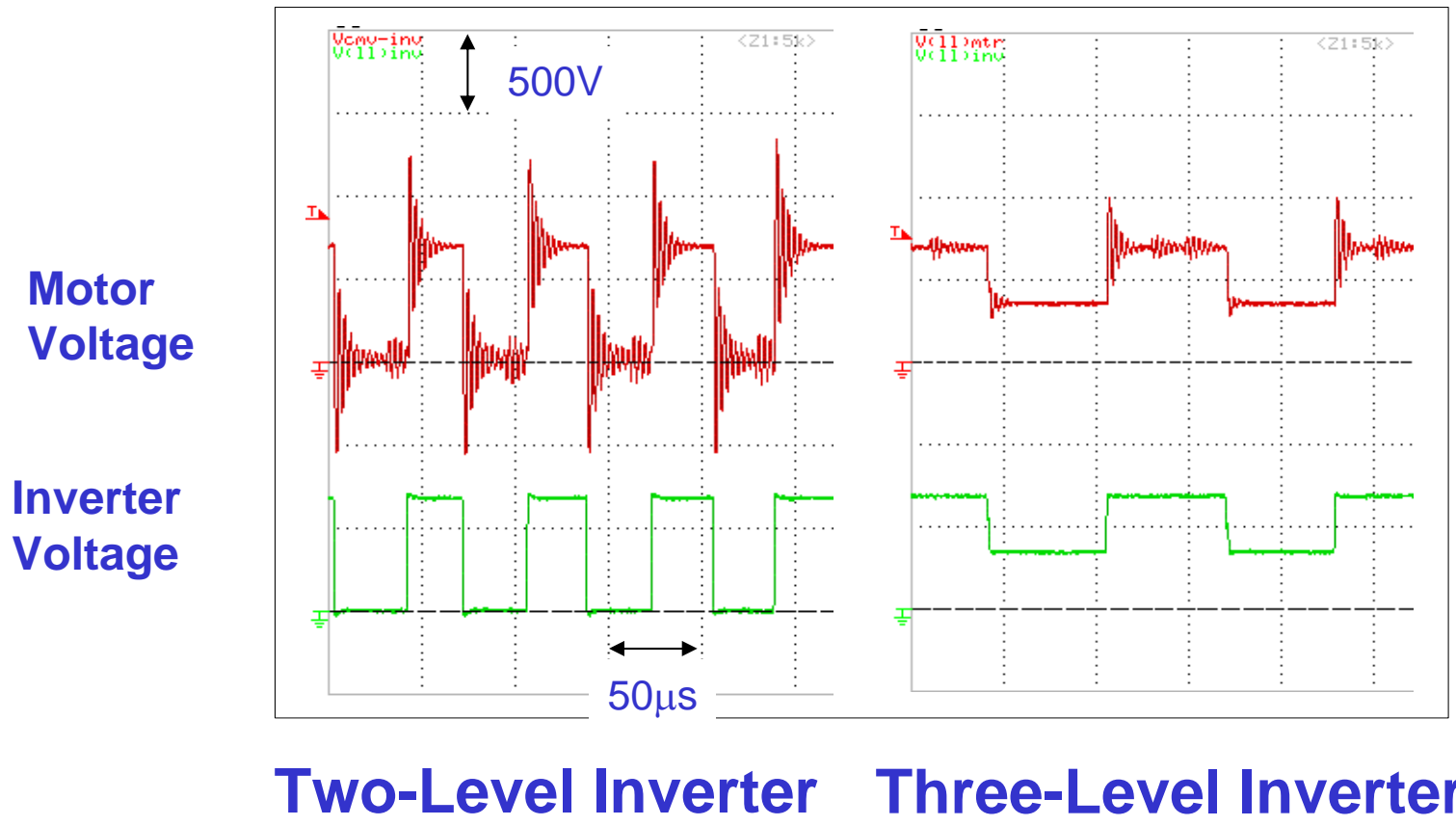
Two-Level Inverter



Three-Level Inverter

10d. Measured Surge Voltage at Motor Terminals

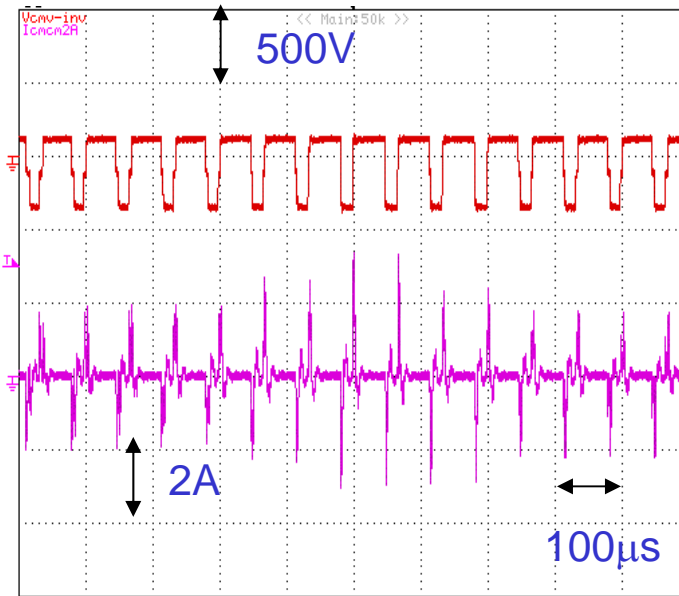
(460V, 7.5 kW with 100m cable)



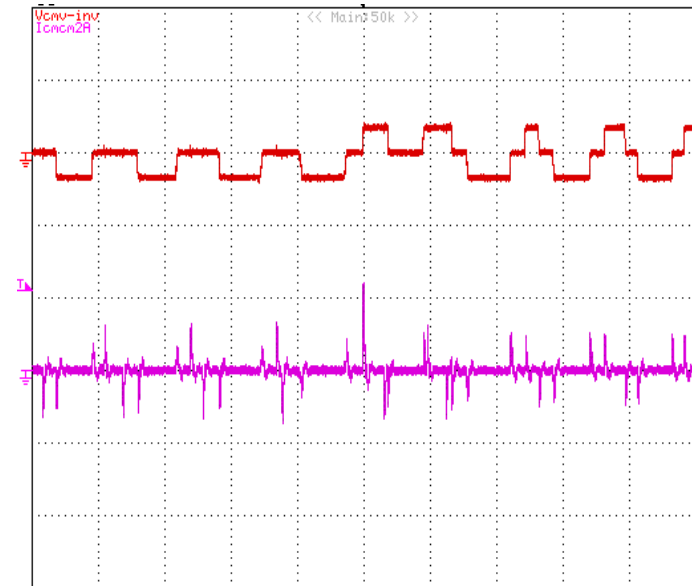
10e. Leakage Current (460V, 7.5 kW with 100m cable)

Common-mode voltage

Leakage current



Two-Level Inverter

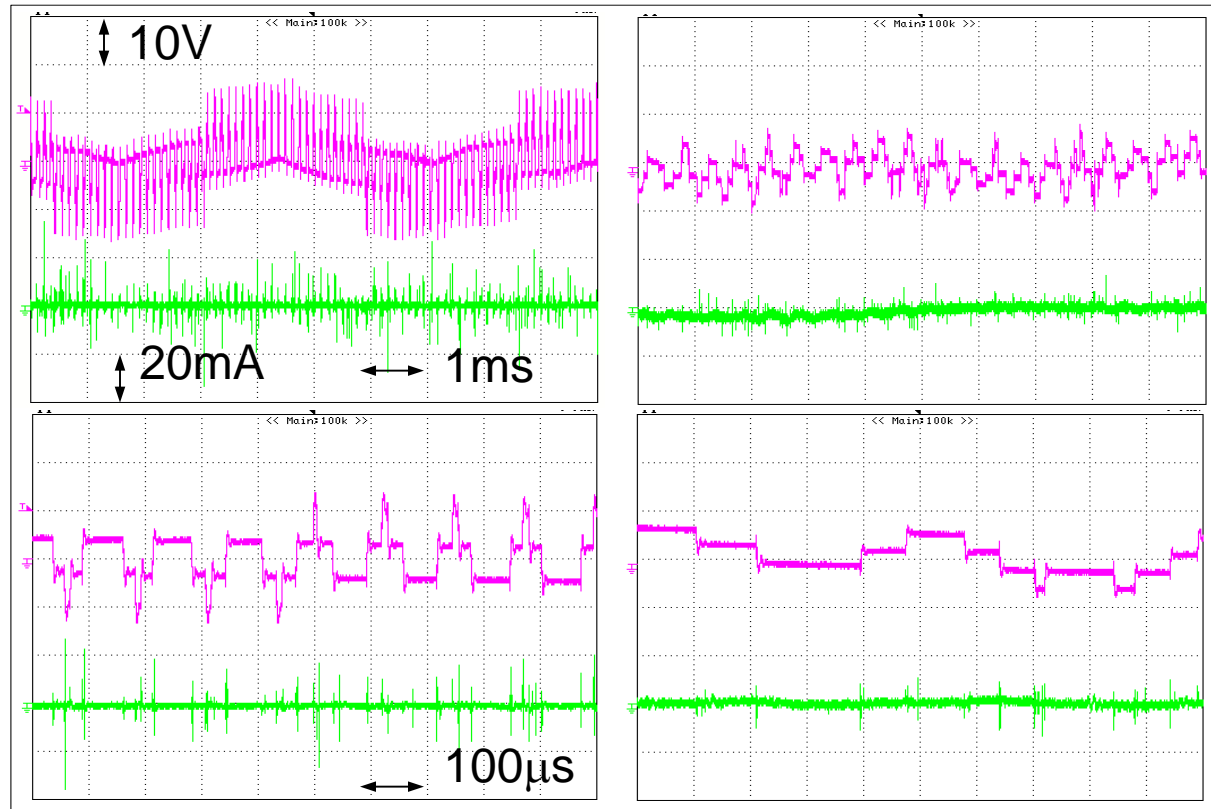


Three-Level Inverter

10f. Shaft Voltage and Bearing Current

Shaft voltage

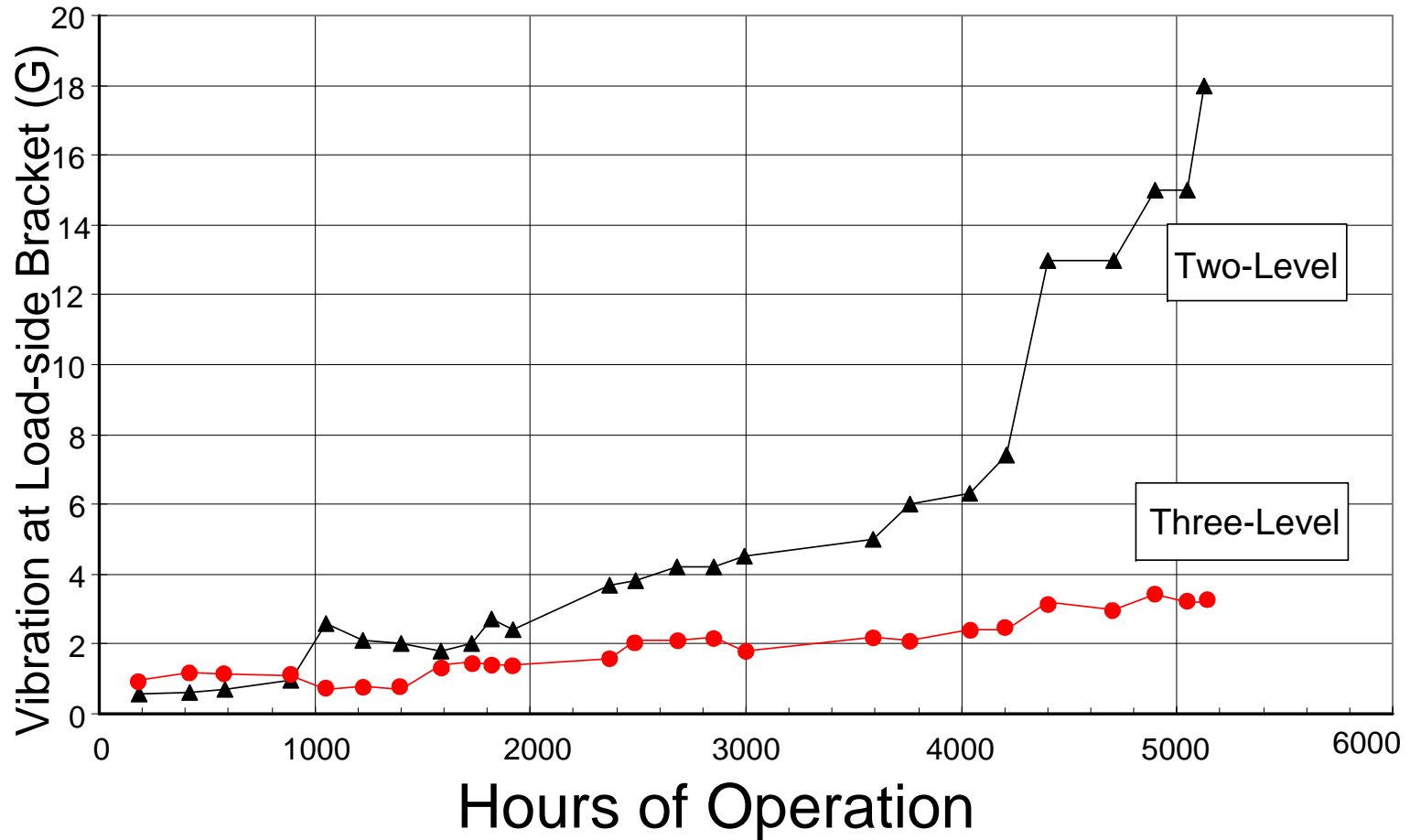
Bearing current



Two-Level Inverter

Three-Level Inverter

11. Bearing Life Test



Bearing life expectancy improves significantly

12. Conclusions

- Bearing insulation characteristics was studied – Level of shaft voltage influences bearing current significantly; Temperature is also very crucial
- Common Mode Filter is helpful when used with 2-level drives to reduce shaft voltage and bearing currents
- 3-Level NPC Inverter is an important tool in mitigating bearing failure – Results in space savings and makes it adaptable to clean room applications; Reduces Surge Voltage as well.